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JULY 2015

HARSH REALITY

The agenda for natural gas

MARKET VOLATILITY

A return to business
-as-usual

A BIG STEP FORWARD ...

... for China-led
development bank

GREEN ENCYCLICAL-

Fix the climate, says
Pope Francis

ENERGY TRANSITION

Exclusive interview

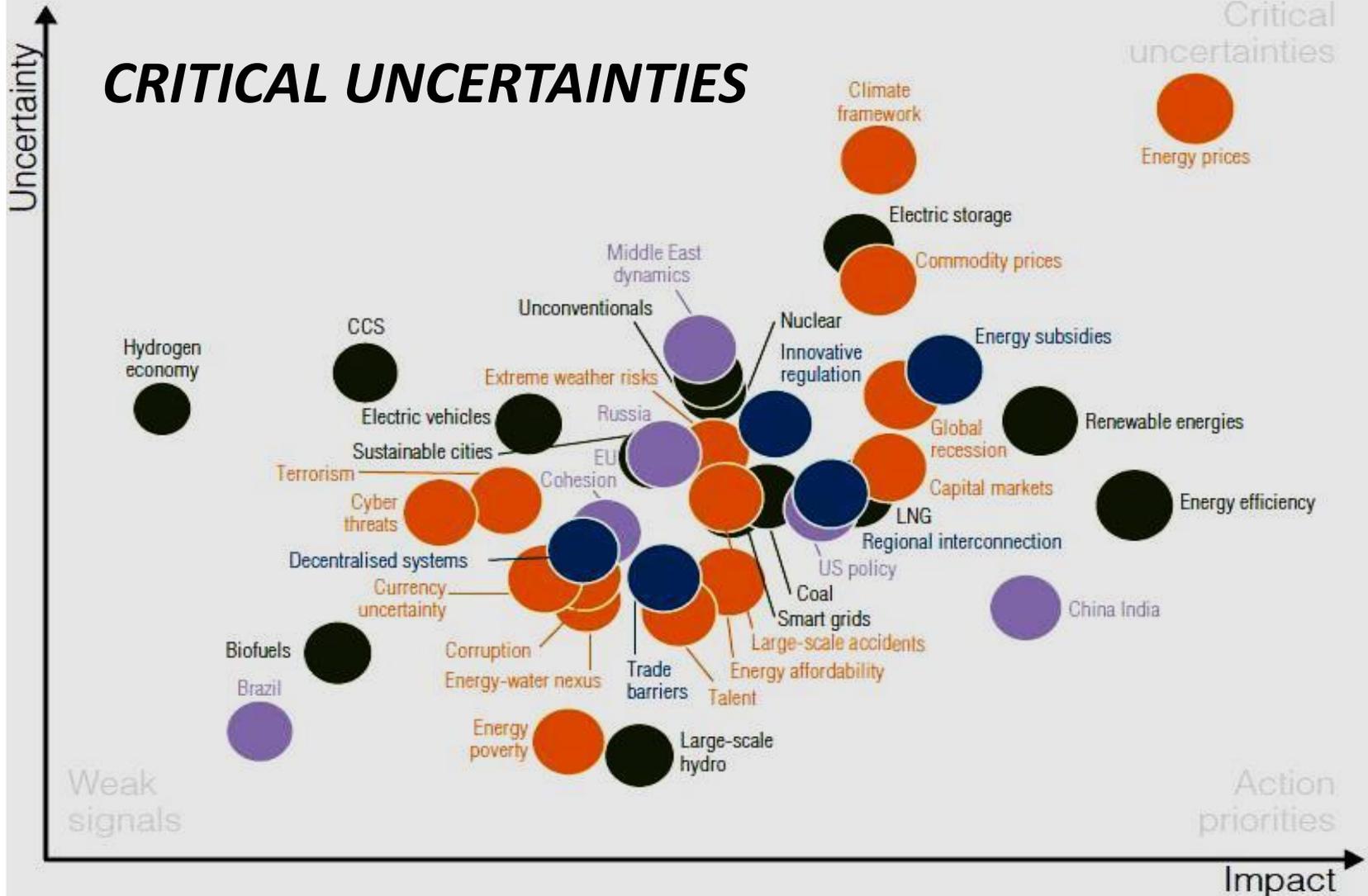
CLIMATE PLEDGES

From China, the US,
Brazil, Korea

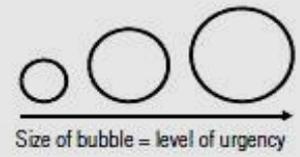
NIGERIA'S OPPORTUNITY

President Buhari
prioritises energy

CRITICAL UNCERTAINTIES



- Macroeconomic
- Business environment



- Geopolitics and regional
- Vision and technology

4th International Symposium on Energy Challenges and Mechanics
- working on small scales
11-13 August 2015, Aberdeen, Scotland, United Kingdom



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Why here?



Why now?



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“Energy Challenges and Mechanics”

**Heterogeneous Electrical and Mechanical Field Effects
in Functional Materials**

**Ken Reifsnider,¹ Fazel Rabbi,² Rassel Raihan,¹ and
Vamsee Vadlamudi²**

1 University of Texas Arlington, UTA Research Center

2 University of South Carolina



4th International Symposium on Energy Challenges and Mechanics
- working on small scales
11-13 August 2015, Aberdeen, Scotland, United Kingdom

Heterogeneous Mechanical and Electrical Field Effects in Functional Materials (for Energy Storage and Conversion)

OUTLINE:

- ❖ Perspectives – Challenges and opportunities
 - ❖ Heterogeneous materials – ‘universal dielectrics;’ membranes as an example
 - ❖ Electrical / mechanical coupling for heterogeneous materials

 - ❖ “Heterogeneous Fracture Mechanics”

 - ❖ Design – Detect – Predict
-

Ken Reifsnider, Univ. Texas Arlington



Multifunctional Heterogeneous (Composite) Materials -

Automotive Industries



Sports Industries

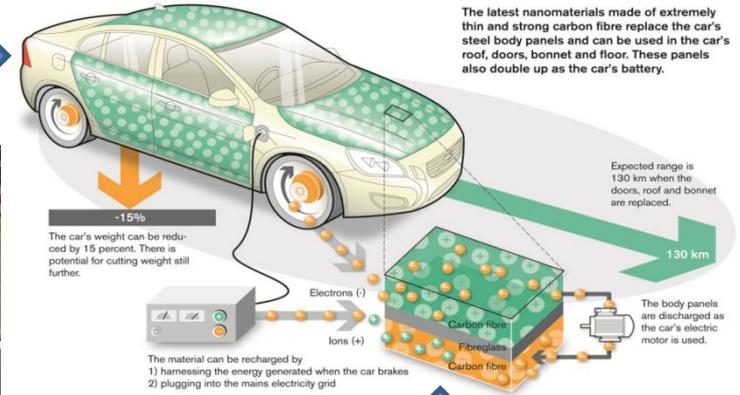


Energy Conversion

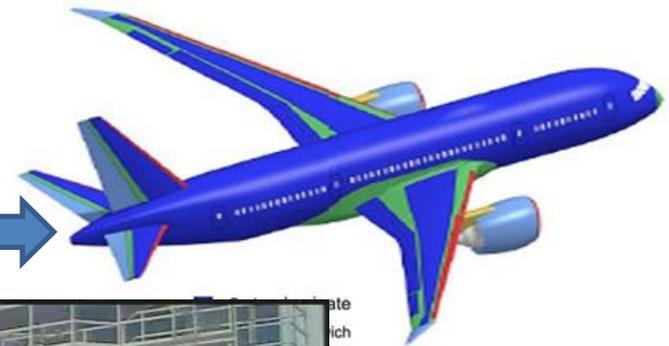
Behavior: Nonlinear?
Non-conservative?

Aerospace Industries

Defense Applications

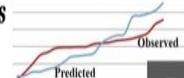


Energy Storage



R. Raihan UTA

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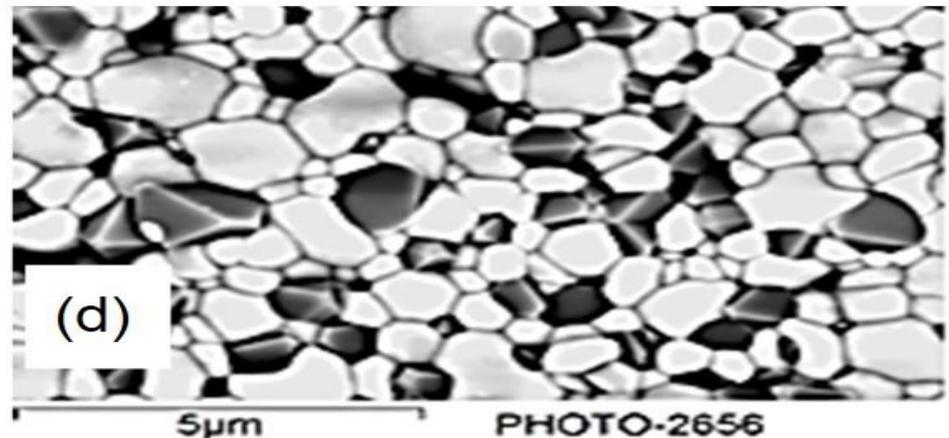
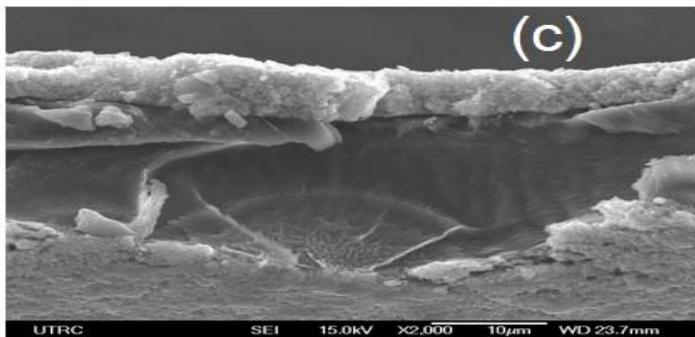
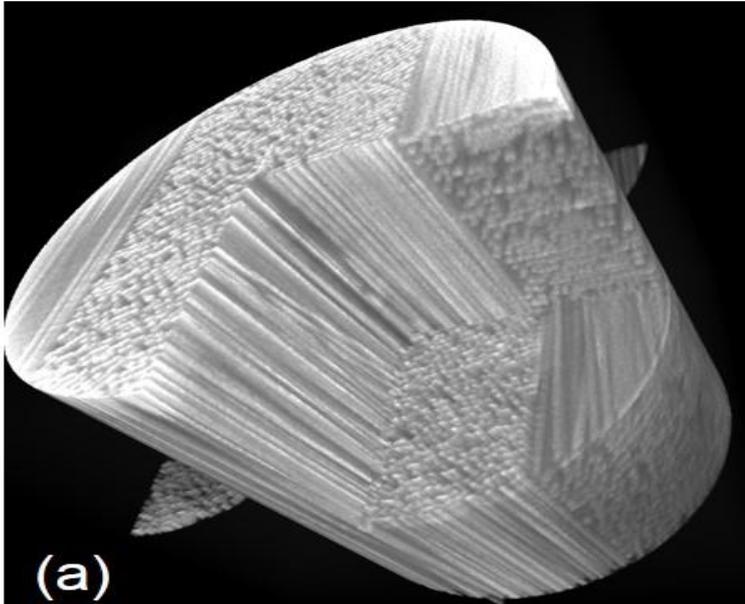
UTARI

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RESEARCH INSTITUTE



Heterogeneous Functional Materials (HeteroFoaM):

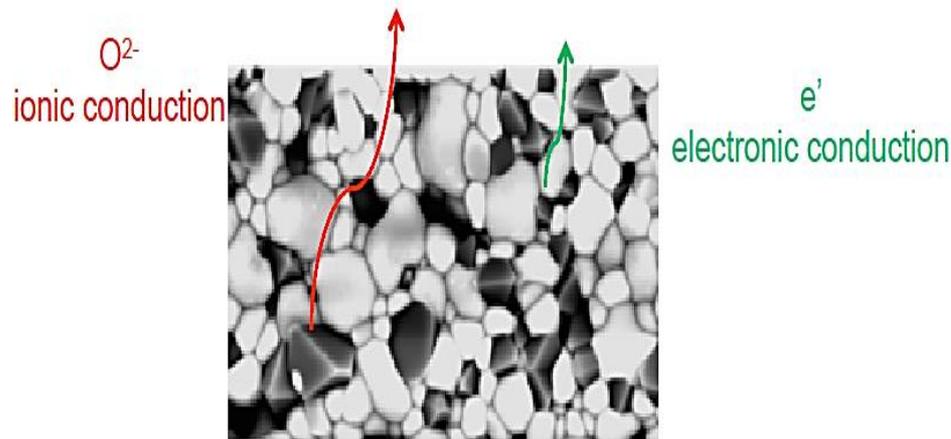
“all heterogeneous materials are fundamentally dielectric”



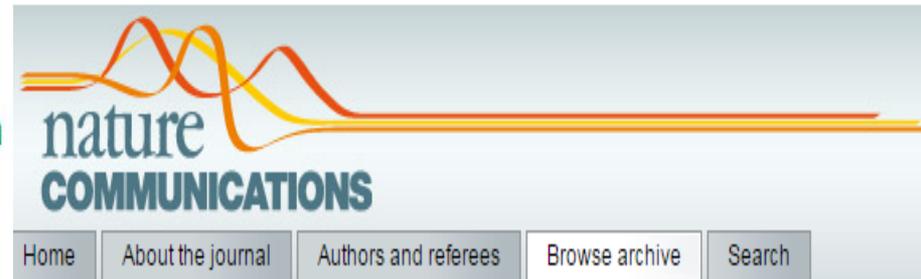
1. K. Reifsnider, W. Chiu, K. Brinkman, Y. Du, A. Nakajo, F. Rabbi, Q. Liu, J. Electrochem. Soc., 160#4, 2013, DOI:10.1149/2.012306jes (HeteroFoaM)

What Should This Picture Look Like?

Including Grain Boundary/Interface Structure and Composition



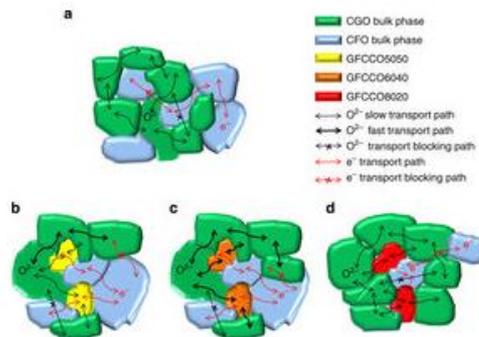
Composite Membranes: for: Nuclear waste management, chemical processing, medical devices,



ature.com > journal home > archive by date > april > abstract

NATURE COMMUNICATIONS | ARTICLE OPEN

Figure 3: Proposed oxygen ionic and electronic transport paths.



(a) Traditional dual phase MIECs (DP-MIECs) without formation of the third phase. (b–d) Novel ternary phase MIECs (TP-MIECs) shown as (b) CGO–CFO5050 (c) CGO–CFO6040 and (d) CGO–CFO8020 in this work.

Enhancing grain boundary ionic conductivity in mixed ionic–electronic conductors

Ye Lin, Shumin Fang, Dong Su, Kyle S Brinkman & Fanglin Chen

Affiliations | Contributions | Corresponding authors

Nature Communications 6, Article number: 6824 | doi:10.1038/ncomms7824

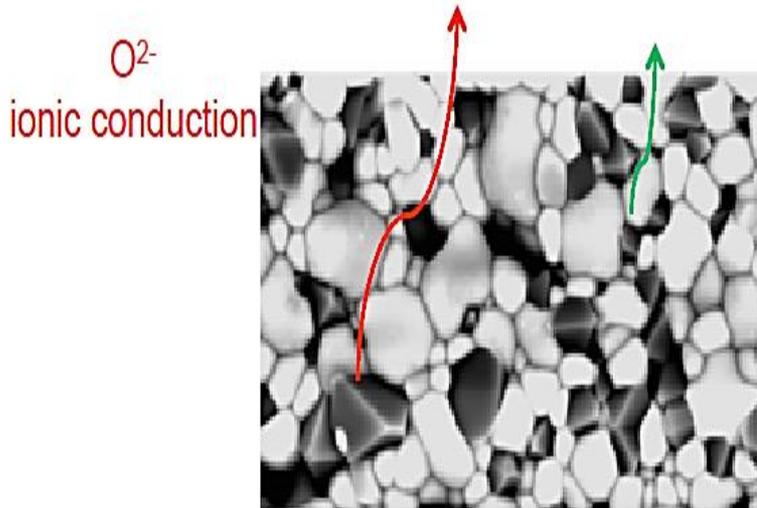
Received 23 September 2014 | Accepted 03 March 2015 | Published 10 April 2015

Mixture or effective property methods cannot capture mechanistic effects or morphology effects:

Including Grain Boundary/Interface Structure and Composition

$$\sigma_i = \sigma_{GDC} \times V_{GDC} + \sigma_{GdFeO} \times (1 - V_{GDC})$$

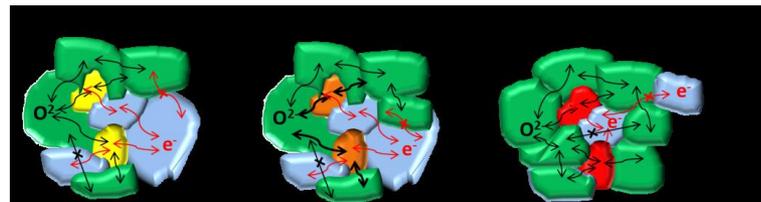
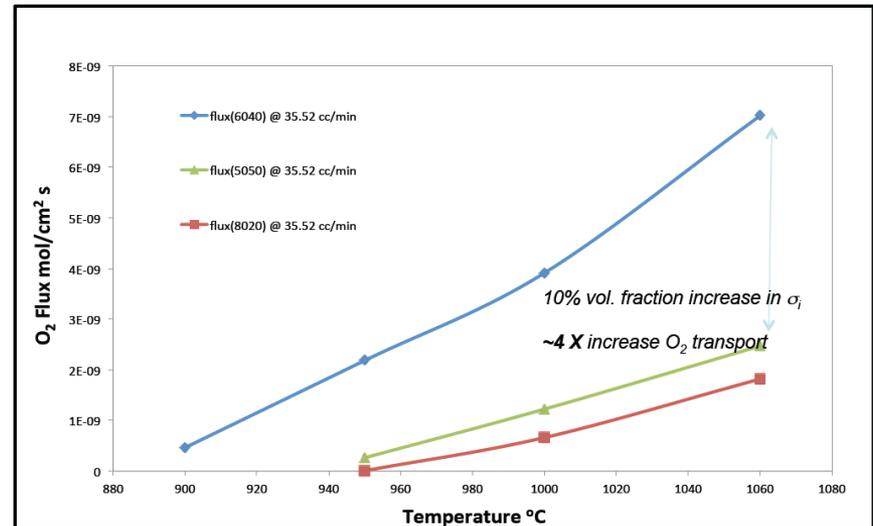
$$\sigma_C = (\lambda - k)\sigma_{elec}V_{elec}^2 + k(\sigma_{elec} - \sigma_i)V_{elec} + \sigma_i$$



e' electronic conduction

$$j_{O_2} = -\frac{RT}{4^2F^2L} \int_{\ln P^I_{O_2}}^{\ln P^II_{O_2}} [\sigma_C] dP_{O_2}$$

Emergent Properties- Role of Microstructure/Interface

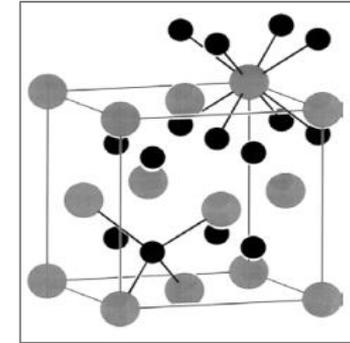


Kyle Brinkman, Clemson
 Fazle Rabbi, U. South Carolina
 Ken Reifsnider, U. Texas Arlington

IONIC PHASE

FLUORITE TYPE

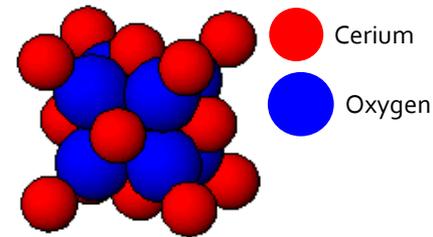
- Calcium fluoride (CaF_2) has a fluorite crystal structure
- **FCC** packing of cations, with anions in all tetrahedral positions
- Also can be described as simple cubic packing of anions with cations in the cubic (8-coordinate) positions



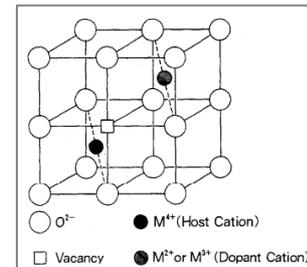
● Fluoride ion
● Calcium ion

GADOLINIUM DOPED CERIA (GDC)

- CeO_2 has the same atomic structure as calcium fluoride
- GDC has a structure similar to CeO_2 with one alternative lattice site filled with ceria and trivalent dopant gadolinium which gives rise to the creation of oxygen vacancies



CeO₂ Fluorite Structure



GDC Fluorite Structure

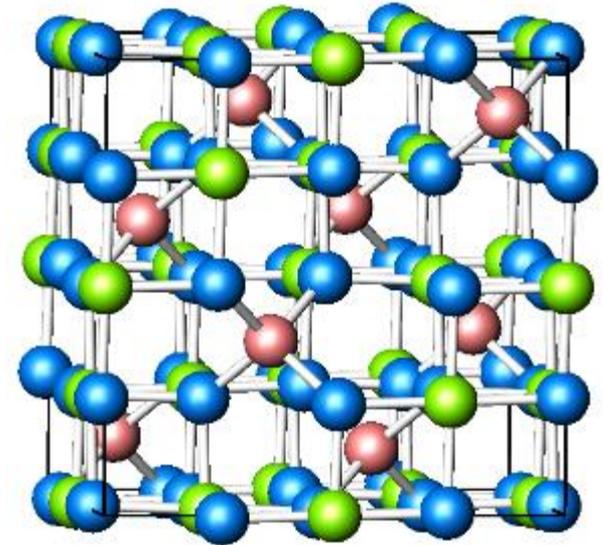
ELECTRONIC PHASE

SPINEL-TYPE MIXED-METAL COMPOSITES

- Spinel type metal oxide can be represented as AB_2O_4 where A is a divalent such as Mg, Fe, Mn, Zn, and Cu.
- B is a trivalent atom Ti, Fe, Al, and Co.
- In a normal spinel structure, all the trivalent cations are located in half of the octahedral sites, while all of the divalent cations occupy 1/8 of the tetrahedral sites.

COBALT FERRITE ($CoFe_2O_4$)

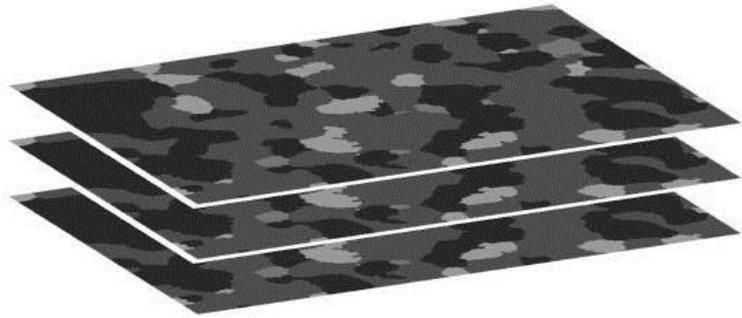
- $CoFe_2O_4$ has an inverse spinel crystal structure.
- In the case of an inverse spinel such as $CoFe_2O_4$, the Co cation occupies one half of the octahedral coordination sites. Half of the Fe^{3+} cations occupy the other half of the octahedral coordination sites as well as all of the tetrahedral coordination sites.



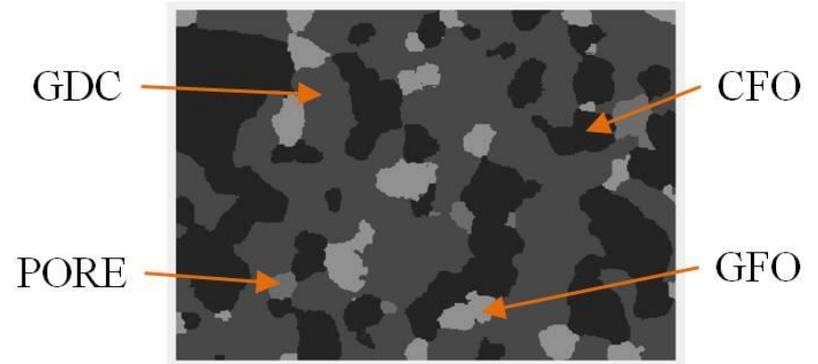
- Oxygen ion
- Cobalt ion
- Iron ion

Crystal Structure of Cobalt Ferrite ($CoFe_2O_4$)

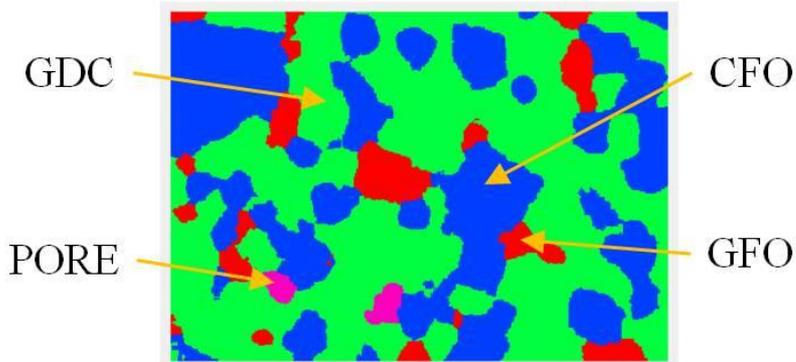
SEGMENTATION



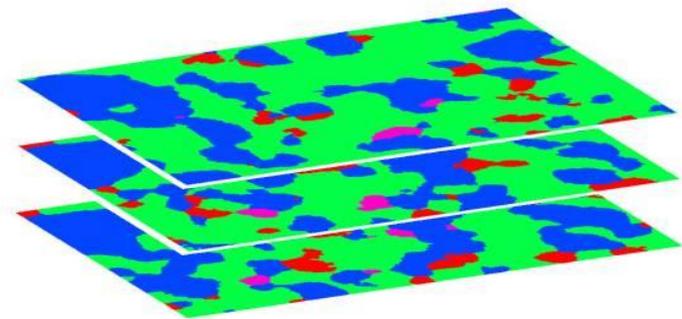
2D image stack obtained from 3D x-ray scan (W. Chiu, UConn)



Grayscale segmentation based on X-ray absorption behavior

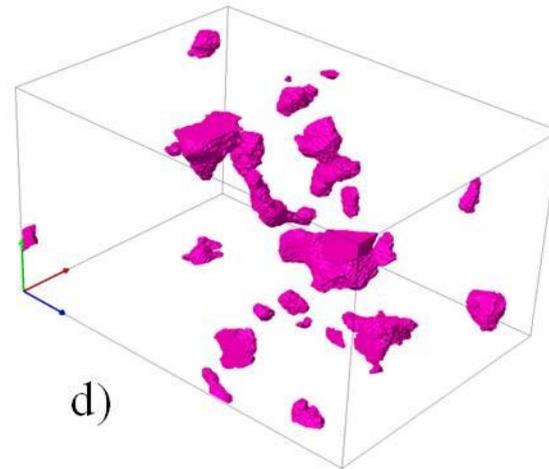
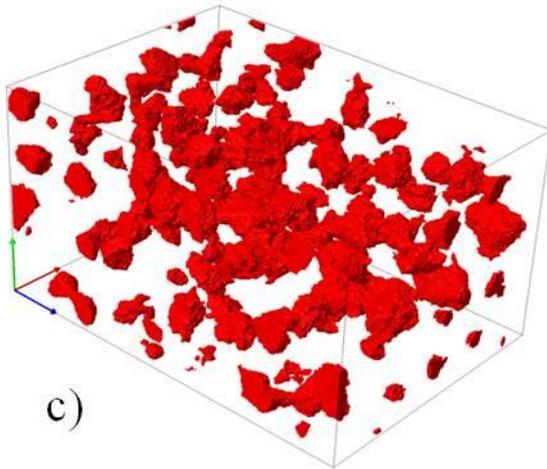
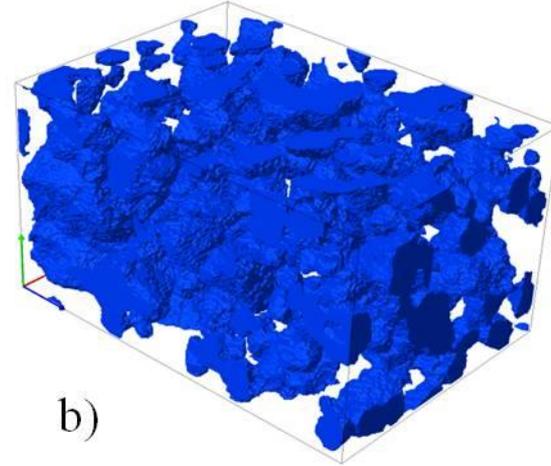
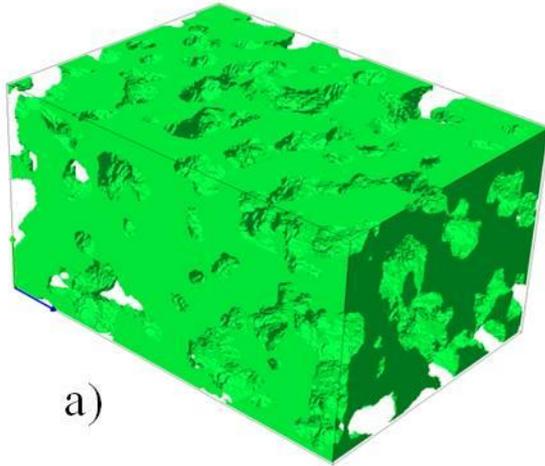


Mask segmentation of different membrane phases based on their grayscale intensity



Stack of segmented mask representing different layer of the membrane structure

3D PHASE REPRESENTATION

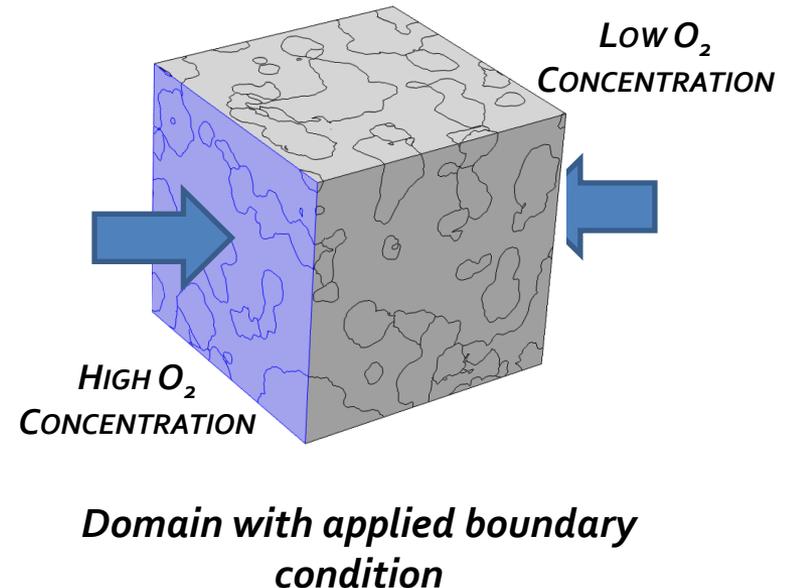


*Three dimensional volume representation of separated constituents of 60%GDC-40%CFO-
a) GDC, b) CFO, c) GFO and d) pore.*

COMPUTATIONAL MODEL

MODEL SETUP

- Concentration gradient is applied as boundary condition on opposing faces
- Other boundaries are kept as chemically and electrically included
- Electric potential can be applied in the boundaries if required in the system
- Individual diffusion properties are applied to the phases
- Negligible contribution from internal boundary between
- Parameter dependent material properties can be used for each phases



TRANSPORT MODEL

NERNST-PLANCK EQUATIONS

$$N_i = -D_i \nabla c_i - z_i u_{m,i} F c_i \nabla \phi_i + c_i \mathbf{u}$$

N_i = Flux of species, i (mol/m².s)

D_i = Diffusion co-efficient (m²/s)

c_i = Concentration of ion, i (mol/m³)

z_i = valance of species

$u_{m,i}$ = mobility (s/mol/kg)

F = Faraday constant

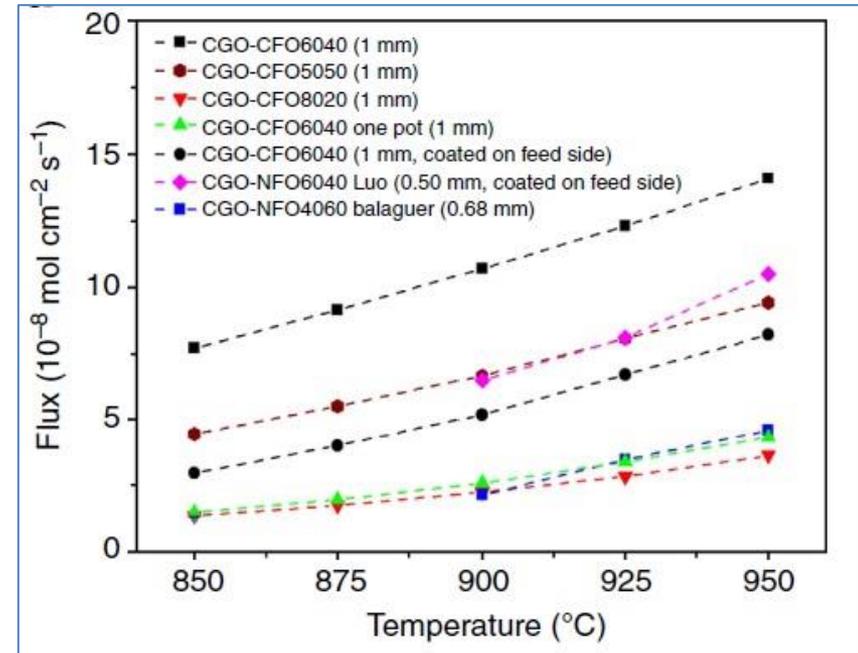
ϕ_i = Electrolyte Potential

\mathbf{u} = velocity vector (m/s)

RESULTS

COMPARISON

- Comparison with reported result by Lin, Y. et al.
- Initial study is with a 6040 GDC-CFO mixture
- Temperature dependent reported value
- The reported result includes grain boundary contribution to total flux

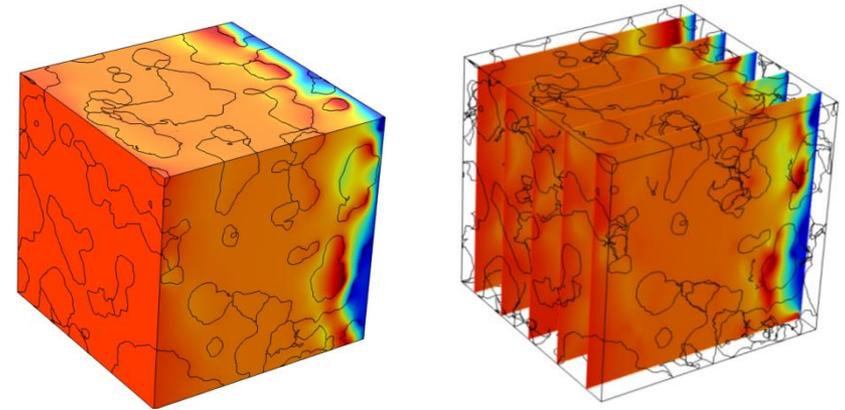


Lin, Y. et al. "Enhancing grain boundary ionic conductivity in mixed ionic–electronic conductors." *Nat. Commun.* 6:6824 (2015).

RESULTS – HOW THE MATERIAL DESIGN CONTROLS THE FUNCTIONALITY

O₂ CONCENTRATION GRADIENT

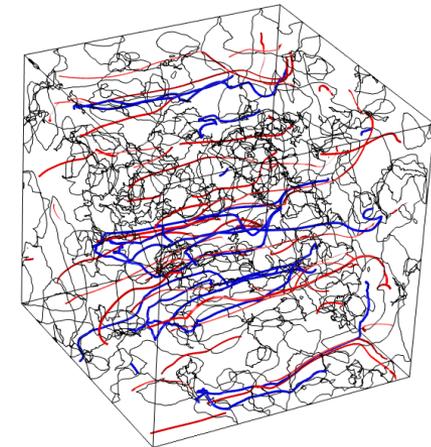
- Concentration gradient of different species is obtained from the model
- Volume plot shows concentration variation across material and boundaries
- Slice plot indicates through – the - thickness concentration gradients



Oxygen ion concentration a) volume plot, b) slice plot

SPECIES TRANSPORT PATH

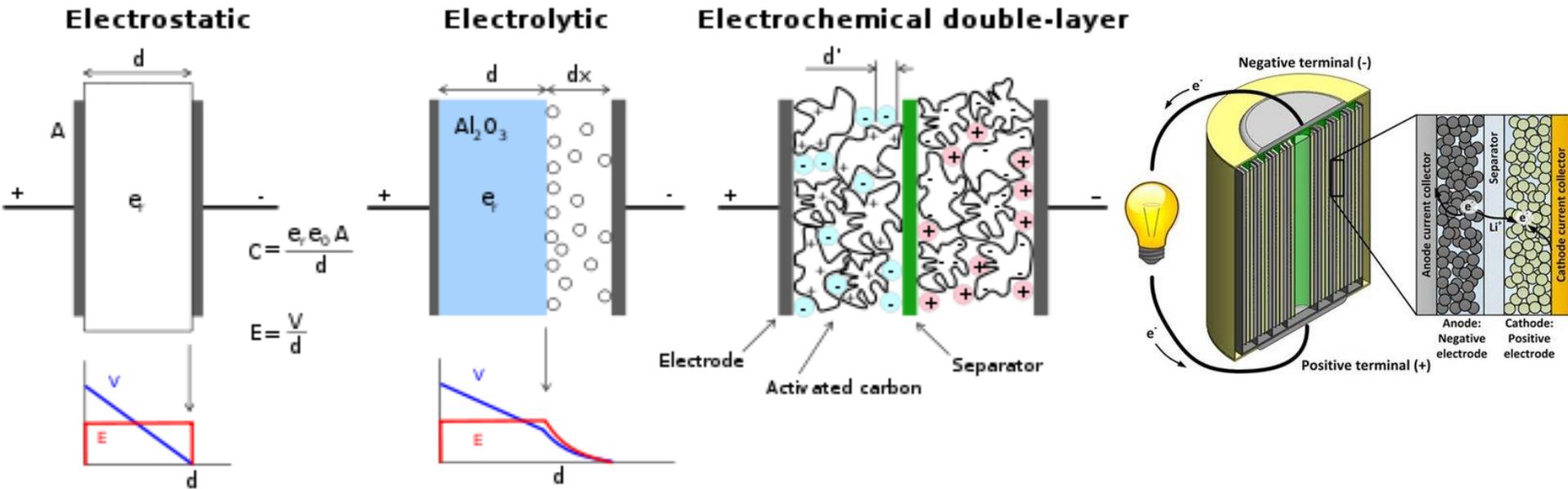
- Species transport paths show flow of two species through the phases
- This can be useful to study the effect of path variation and morphology on the overall flux transport
- Integral of transport path can be obtained to calculate ion travel distance through the membrane



Oxygen ion concentration a) volume plot, b) slice plot

“Universal Dielectrics”

Charge displacement → Capacitance in HeteroFoam materials - some fundamental understandings:



The local properties, shapes, and mobilities determine the dielectric response

ANALYSIS: DIELECTRIC BEHAVIOR OF COMPOSITE MATERIALS

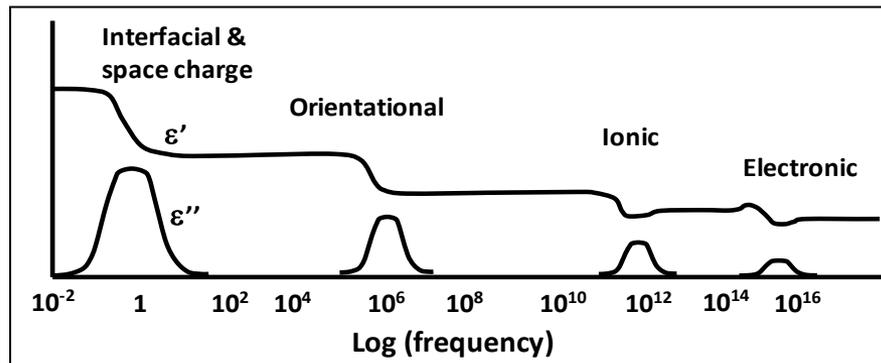
- Embedded boundary method, closed form; representative volume element
 - Comsol Multiphysics AC/DC module was used for computational
- Maxwell's equations and continuity of charge:

$$-\nabla \cdot d((\sigma + j\omega\varepsilon_0)\nabla V - (\mathbf{J}^c + j\omega\mathbf{P})) = d\mathbf{Q}_j$$

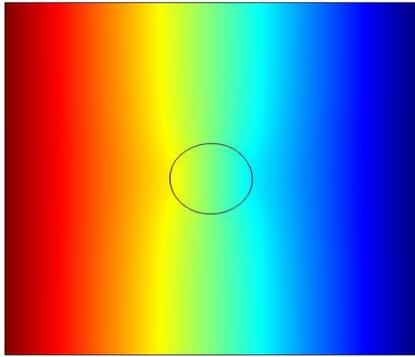
- with no internal current source and charge density

$$-\nabla \cdot d((\sigma + j\omega\varepsilon_0)\nabla V) = 0$$

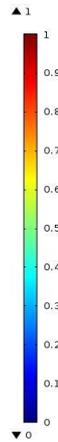
- **Time-variable current** is applied on the input port to measure impedance response.
- Frequency varied from **0.1Hz-1MHz**.
- Frequency dependent single phase material properties can be applied to corresponding material domain for each different frequency.
- Frequency dependent material properties-Obtained by **NOVOCONTROL™**.



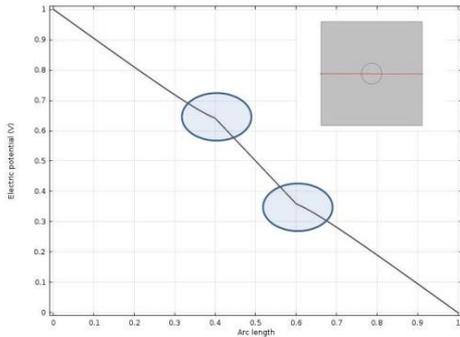
Surface charge: determined by the jump in the gradient of the potential



Potential distributions around the inclusion

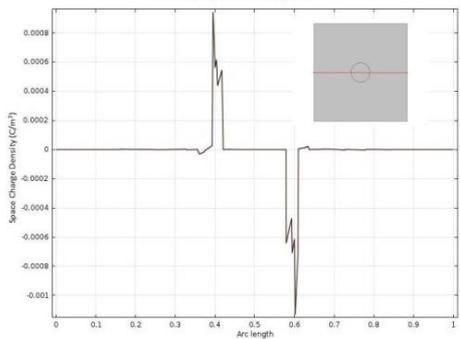


Line Graph: Electric potential (V)



Potential distributions along the line

Line Graph: Space charge density (C/m²)



Space charge densities along the line

Surface Charge Density

The surface charge density on a solid is defined as the total amount of charge q per unit area A ,

$$\sigma = \frac{q}{A}. \quad (1)$$

The surface charge on a surface S with surface charge density $\sigma(\mathbf{r})$ is therefore given by

$$q = \int_S \sigma(\mathbf{r}) d^3 \mathbf{r}. \quad (2)$$

In cgs, Gauss's law requires that across a boundary

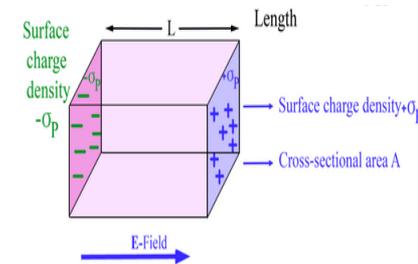
$$(\mathbf{E}_1 - \mathbf{E}_2) \cdot \hat{\mathbf{n}} = 4\pi\sigma, \quad (3)$$

where \mathbf{E}_i is the electric field in medium i and $\hat{\mathbf{n}}$ is the unit normal vector, which is equivalent to

$$\frac{\partial V_1}{\partial r} - \frac{\partial V_2}{\partial r} = -4\pi\sigma,$$

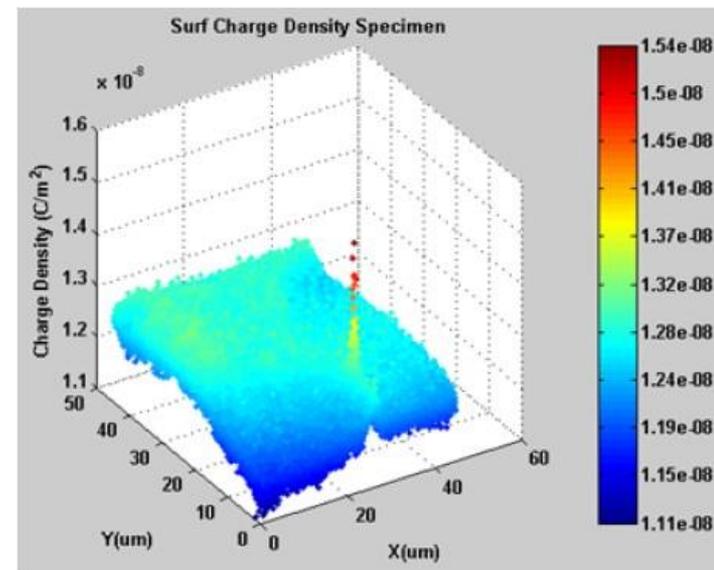
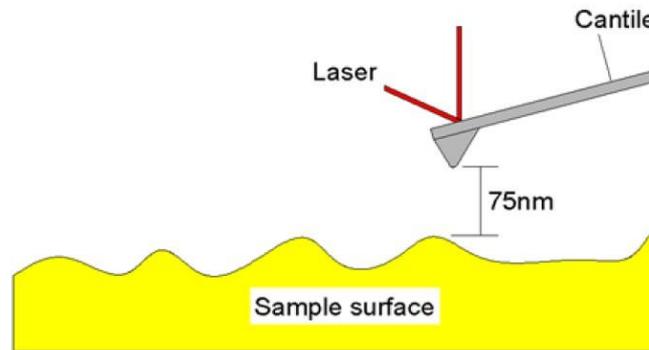
where V_i is the voltage in medium i . Similarly, in MKS,

$$(\mathbf{E}_1 - \mathbf{E}_2) \cdot \hat{\mathbf{n}} = \frac{\sigma}{\epsilon_0},$$

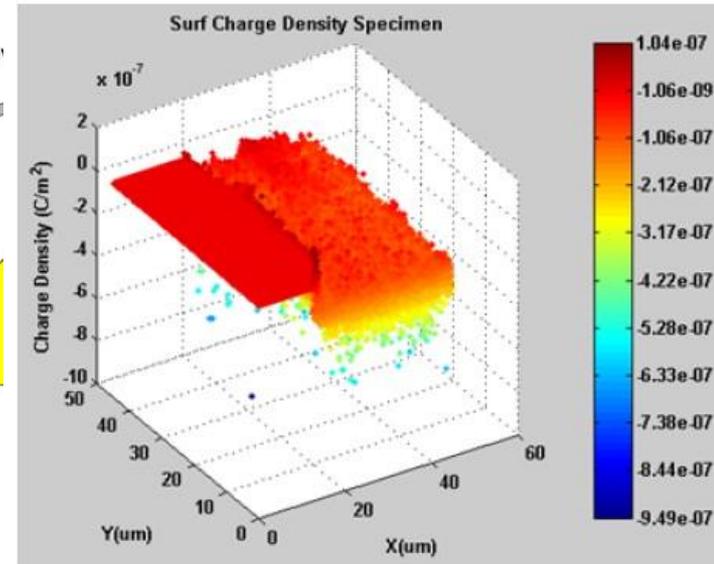


Surface charge: confirmation - EFM Internal

- Cantilever on first pass is at set at 75nm from sample surface and topography data is collected.
- On the second pass the cantilever is backed away and measures electrical properties



(a)



(b)

Fig. 15. (a) Measured surface charge density in the polarization regions on the left on the sample interface ($+1.2e-8\text{C/m}^2$), (b) right ($-9.66e-8\text{C/m}^2$) of the circular inclusion for an applied specimen bias voltage of 10 V.

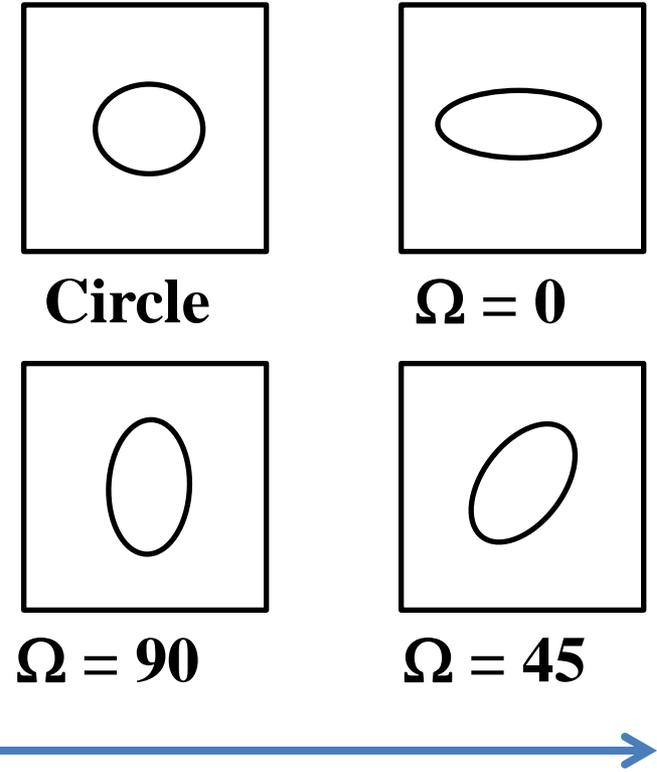
* K. L. Reifsnider, F. Rabbi, J. Baker, J.-M. Adkins and G. Liu, Processing-property relationships in advanced multi-functional composite materials: Management of dielectric behavior, Proc. Int. Conf. Processing and Manufacturing of Advanced Materials, 2–6 December 2013.

* K. L. Reifsnider, Q. Liu, J.-M. Adkins, J. Baker, F. Rabbi and K. Brinkman, Relationship of micromorphology to charge storage and transfer properties in heterogeneous functional materials, Proc. World Conf. Computational Mechanics, 13–18 July 2012.

Physics Based Heterogeneous Non-dilute Material Models

Consider solutions to the non-dilute problem for defect second phases with the following geometries and orientations:

- vary size → volume fraction
- vector electromagnetic field applied
- Systematic variation of orientation



$$-\nabla \cdot d((\sigma + j\omega\epsilon_0)\nabla V) = 0$$

$$\mathbf{D} = \epsilon_0 \epsilon \cdot \mathbf{E}$$

$$\epsilon = \epsilon' + \frac{\sigma}{i\omega\epsilon_0}$$

(1)

non-dilute, heterogeneous

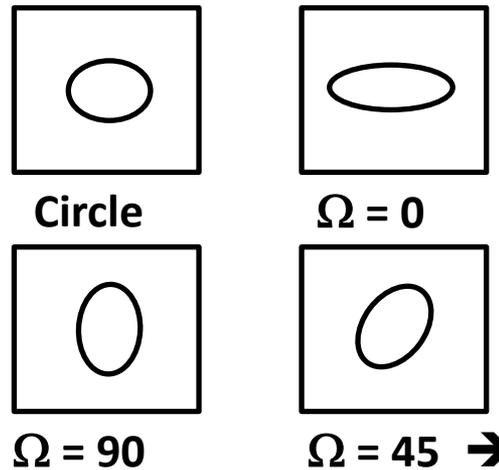
Dielectric property emergence:

Frontier Science → models/validation → material design tools & demos

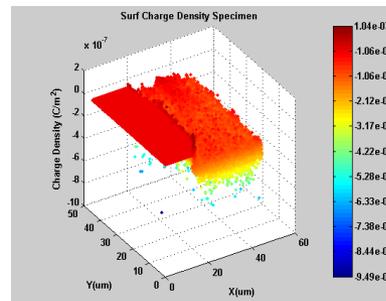
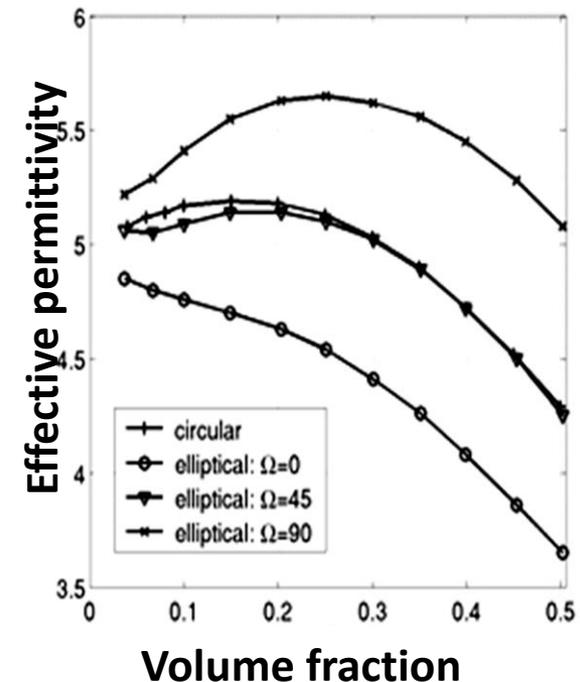
$$-\nabla \cdot d((\sigma + j\omega\epsilon_0)\nabla V) = 0$$

Conceptual innovation:
Construct design tools to predict compliance with multiphysics (mechanical and electrical) applied fields during non-conservative state changes:

New closed form, non-dilute model of material state changes caused by micro-defect accumulation in heterogeneous materials predicts unexpected non-monotonic variations.



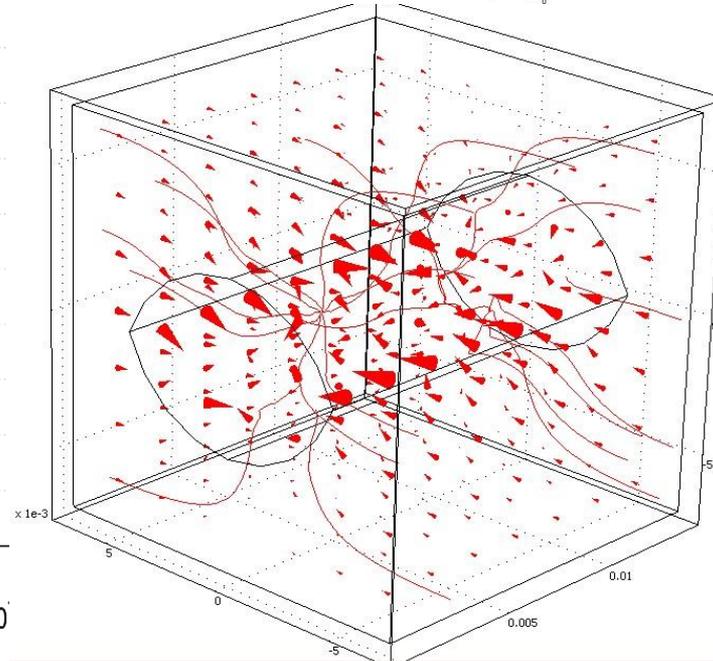
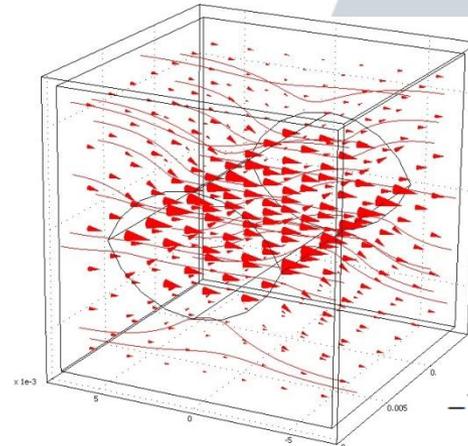
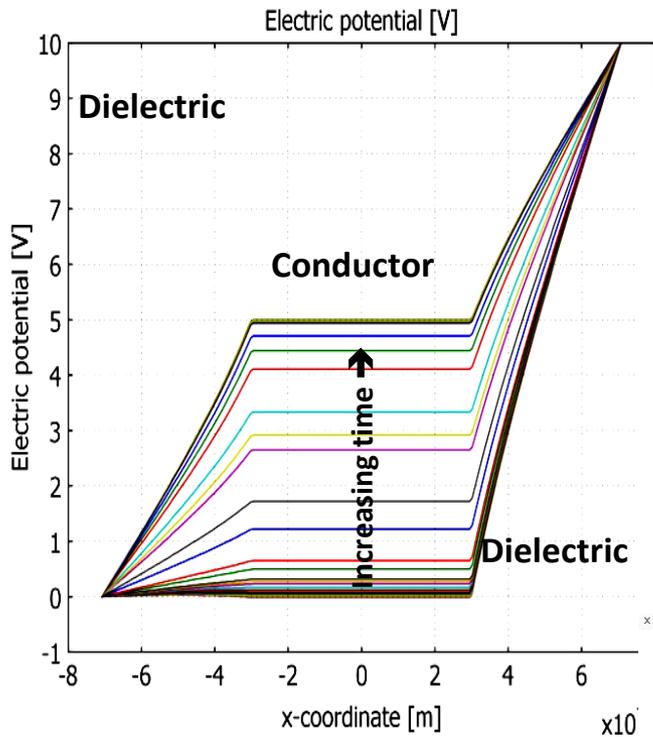
First principles dielectric design



- * Meso-Design of heterogeneous dielectric material systems: structure property relationships, Baker, Adkins, Rabbi, Liu, Reifsnider, and Raihan, J. Advanced Dielectrics, 3#1 (2013)
- * Heterogeneous mixtures of elliptical particles: directly resolving local and global properties and responses, Q. Liu and K. Reifsnider, Journal of Computational Physics (2012), doi: <http://dx.doi.org/10.1016/j.jcp.2012.09.039>

Charge displacement:

We can follow where the current is flowing and where the charge accumulates as a function of time:

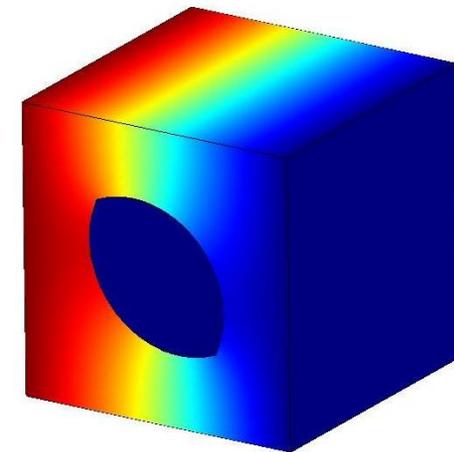


Equations solved:

$$-\nabla \cdot d[(\sigma + j\omega \cdot \epsilon_0) \nabla V - (J^c + j\omega P)] = dQ_j$$



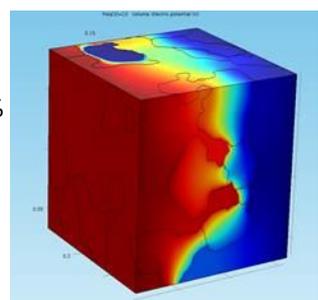
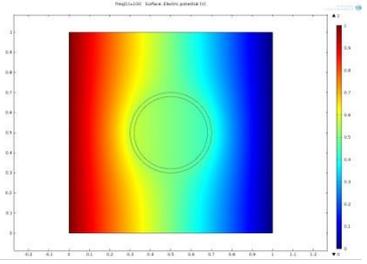
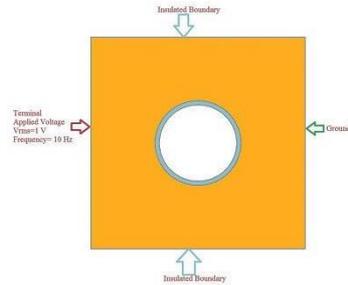
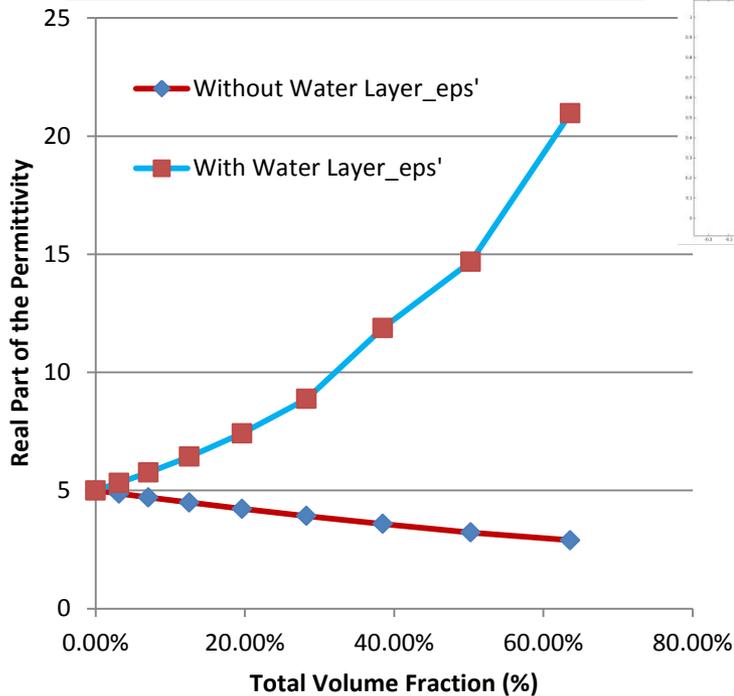
$$-\nabla \cdot d[(\sigma + j\omega \cdot \epsilon_0) \nabla V] = 0$$



Variation of real part of the permittivity with increasing volume fraction at different frequencies

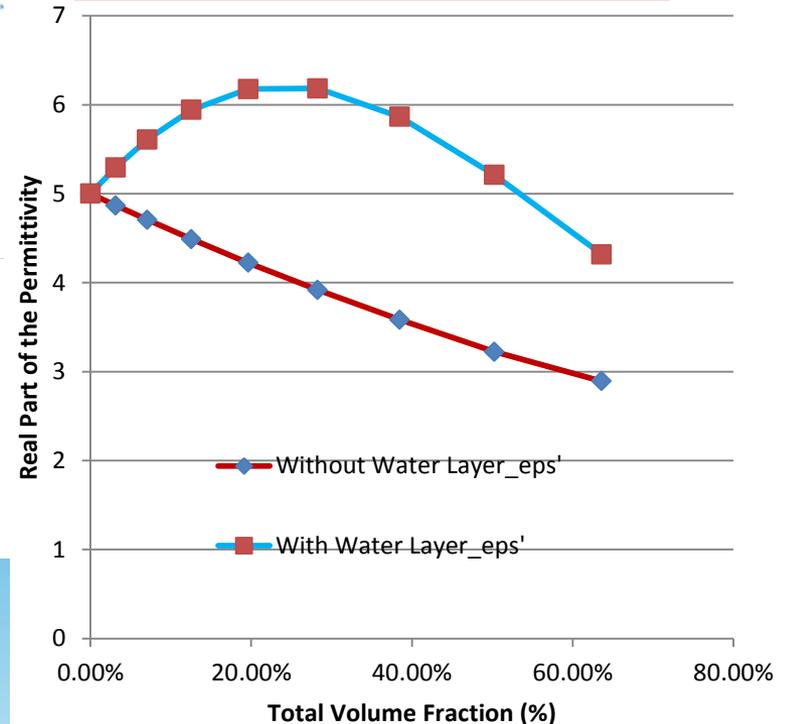
Real Part of the Permittivity vs Total Volume Fraction of the Inclusion

f= 10.8 Hz
 σ (Conductive Layer) = $1E-6.1$ S/m
 ϵ_r (Conductive Layer) = 10



Real Part of the Permittivity vs Total Volume Fraction of the Inclusion

f= 100 Hz
 σ (Conductive Layer) = $1E-6.1$ S/m
 ϵ_r (Conductive Layer) = 10

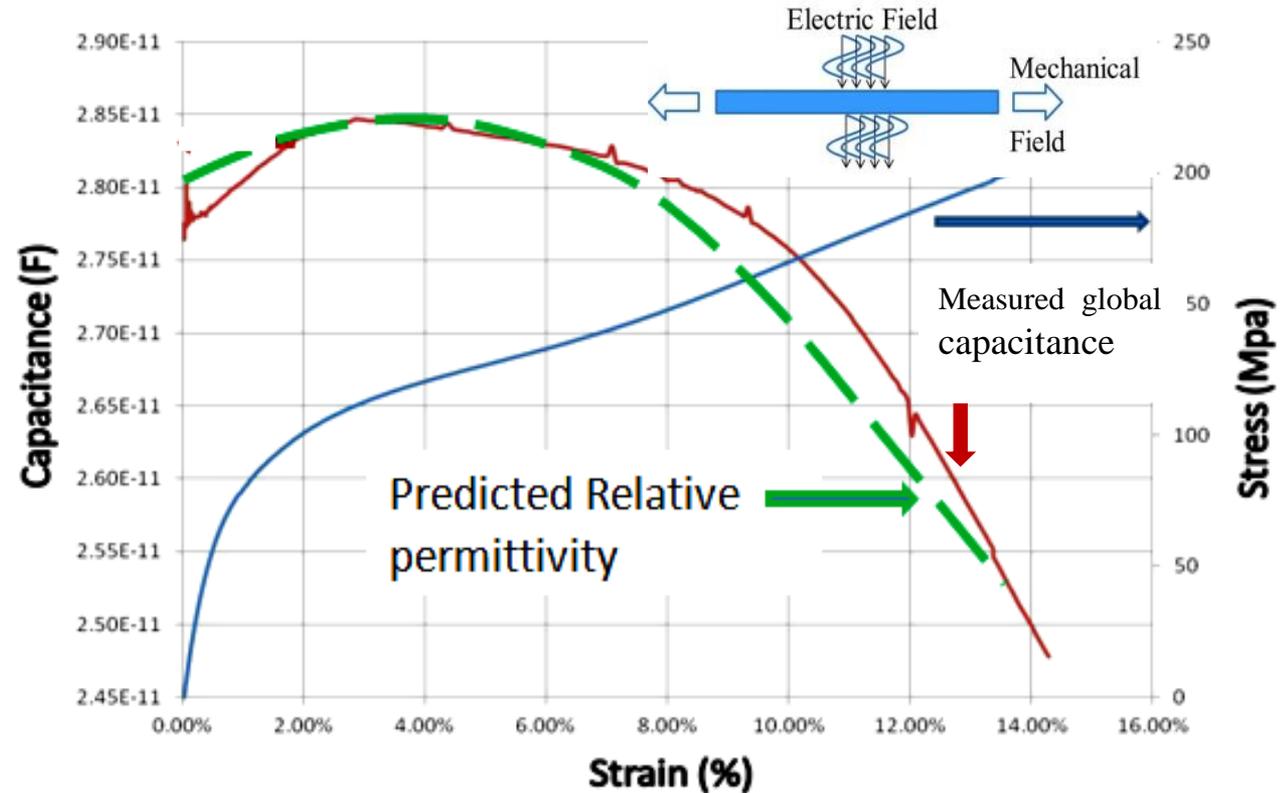


Concept of generalized compliance to fields (mechanical and electrical) –

Validation:

Experiments validate global predictions of general compliance for local non-conservative material state changes caused by mechanical + electrical fields.

New tool for Material State Awareness that discriminates specific local details of damage for non-dilute accumulation of defects.

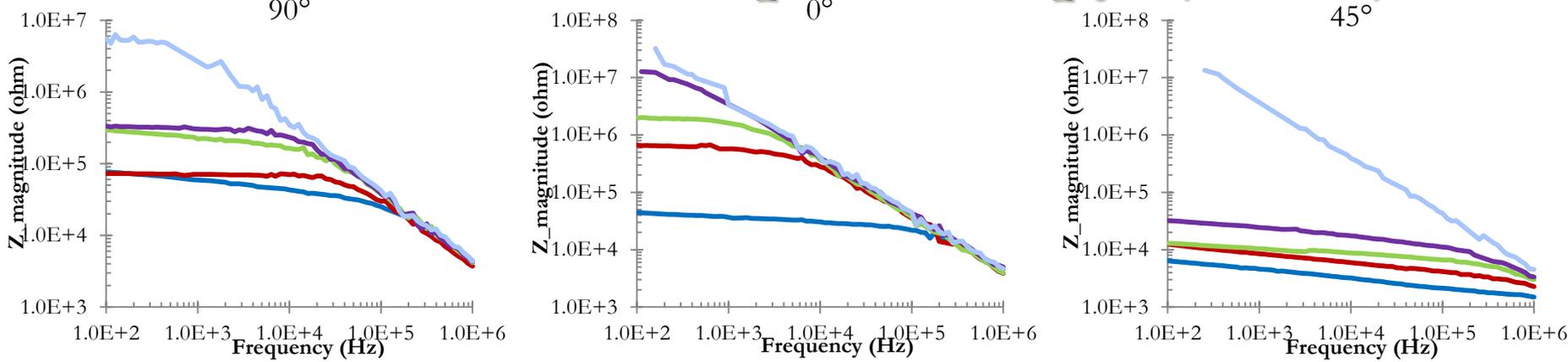


MULTIPHYSICS DESIGN AND DEVELOPMENT OF HETEROGENEOUS FUNCTIONAL MATERIALS FOR RENEWABLE ENERGY DEVICES: THE HeteroFoam STORY, J. Electrochemical Society, accepted, (2013), Keynote lecture, ECS Prime, 2012 K. Reifsnider (USC), Y. Du, Wilson Chiu(UConn), Kyle Brinkman(SRNL),

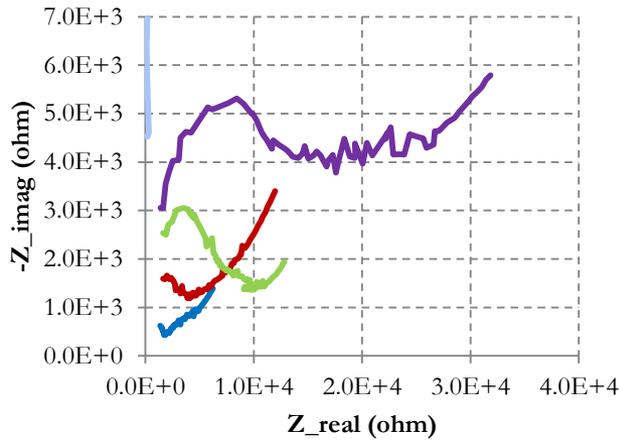
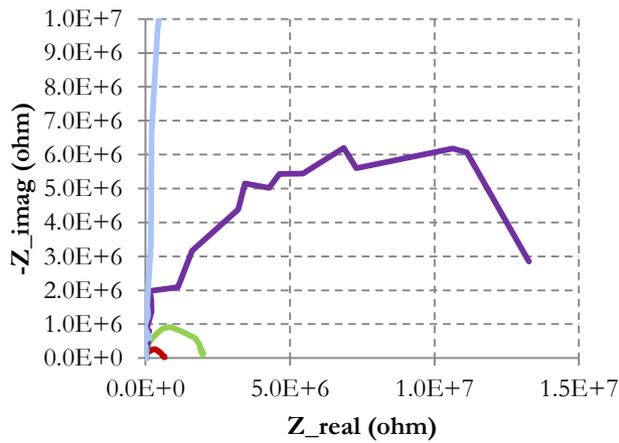
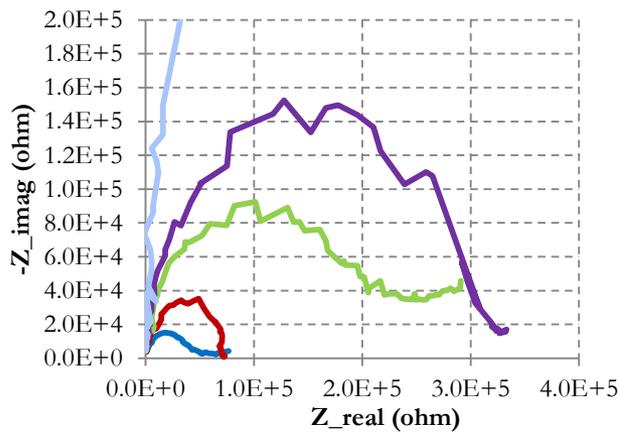


Fatigue: Physics Based Damage Models

Broadband Dielectric Spectroscopy (BbDS)

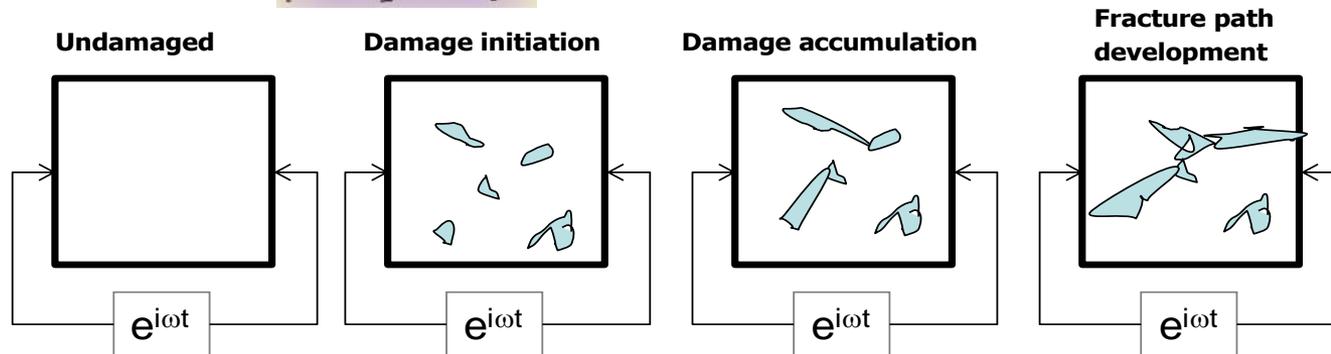
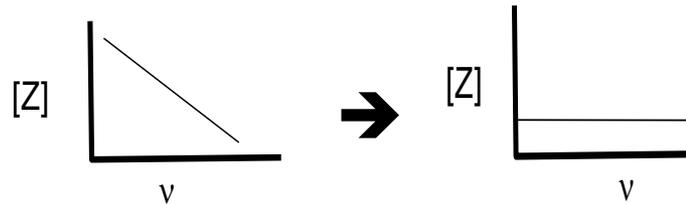
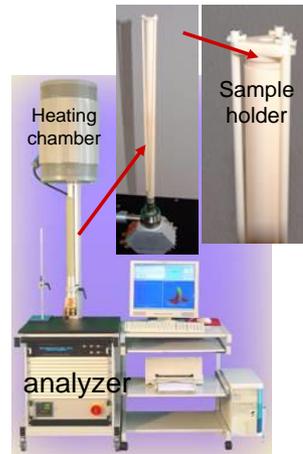


— n/N = 1 — n/N = 0.75 — n/N = 0.50 — n/N = 0.25 — n/N = 0



Characterization and sensor technology:

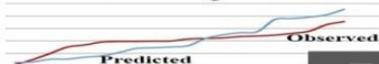
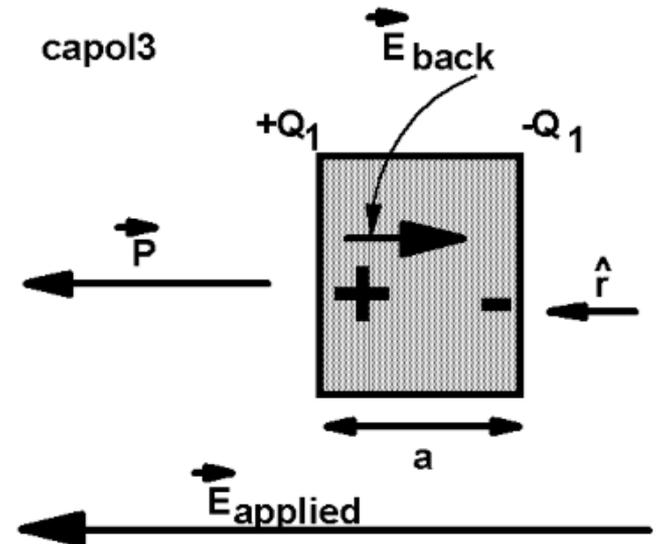
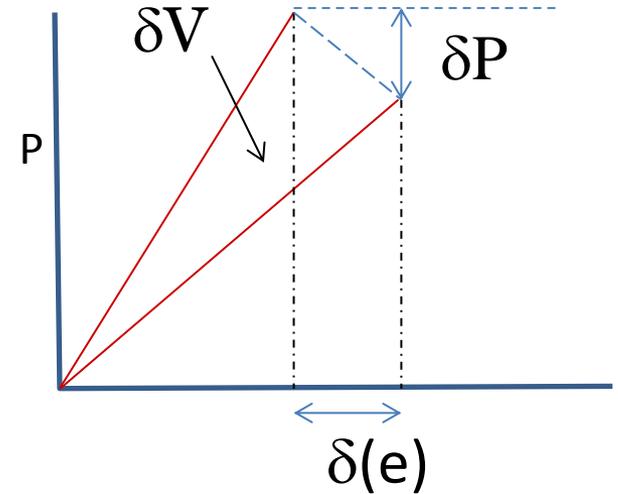
Physics Based Damage Models for Materials State Awareness:



K. Reifsnider, P. Majumdar & P. Fazzino, "Material State Changes as a Basis for Prognosis in Aeronautical Structures," J. Aeronautical Society, Vol. 113 #1150 (2009) **Silver award winner.**

Premise:

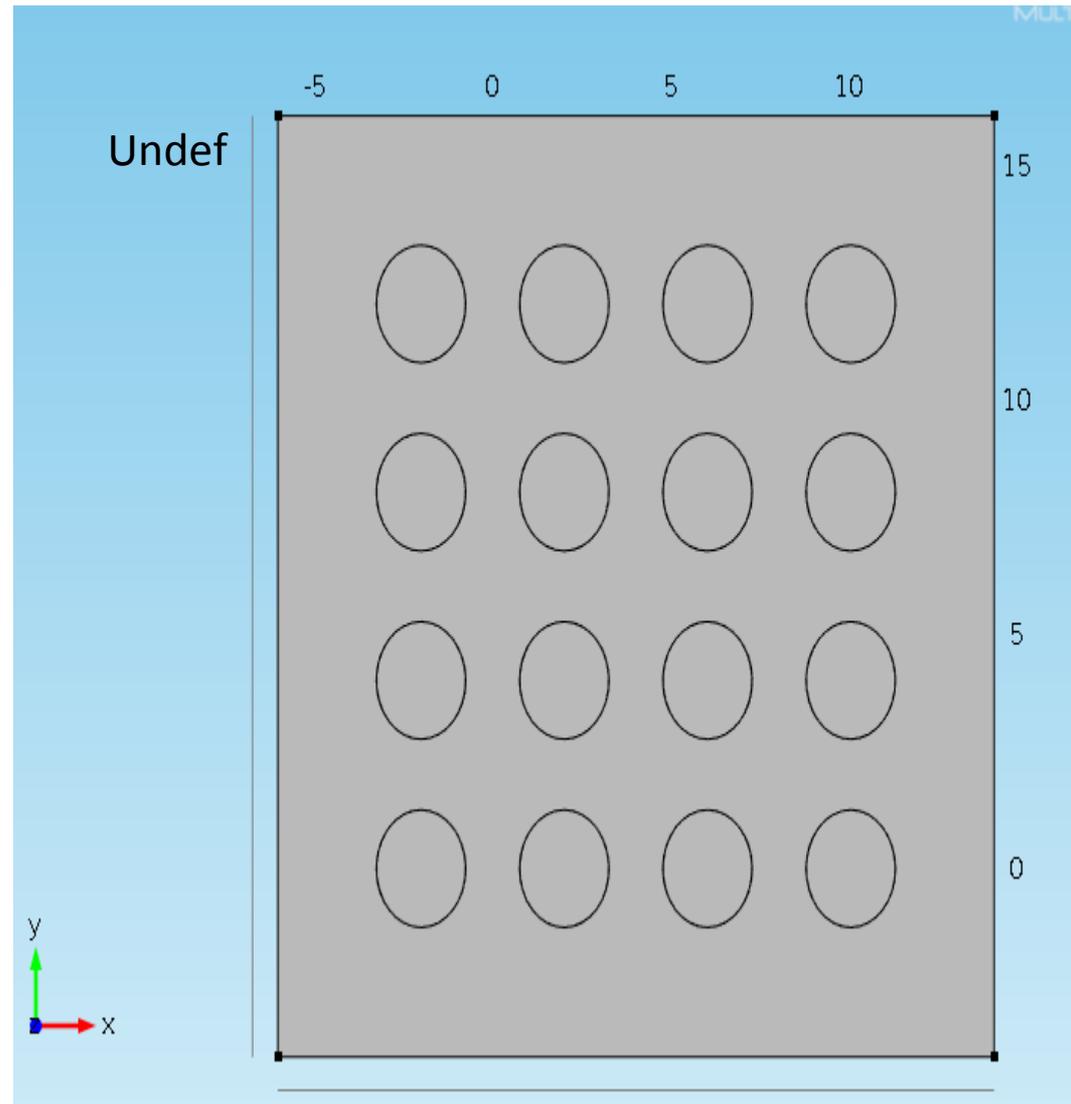
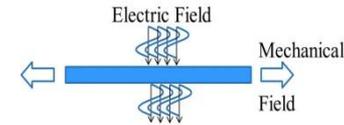
- ❖ We can use dielectric state variable(s) to relate material response to mechanical and electric fields
- ❖ Those state variables have the advantage of integrating and correctly interpreting the collective, emergent effect of complex damage / material state changes
- ❖ The foundations of that capability are evident, rigorous, and invertable (as a foundation for design).



Can we demonstrate the basic foundations?

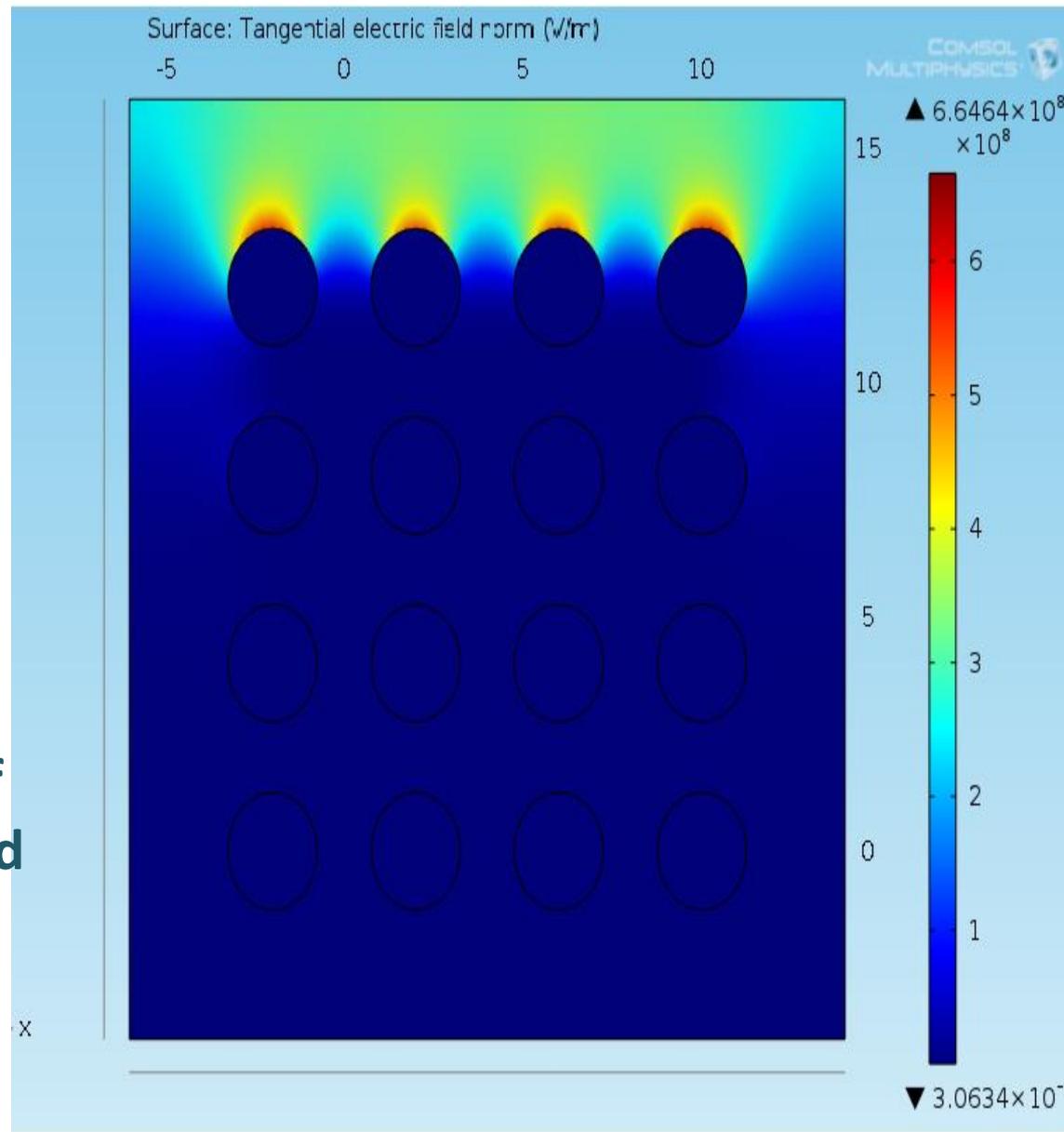
Nonlinear deformation:

- ❖ Horizontal mechanical field (ABAQUS)
- ❖ Vertical electrical field (COMSOL)
- ❖ Can we make a 1:1 association between the distinguishing features of damage development and changes in dielectric properties, e.g., capacitance?



Nonlinear deformation:

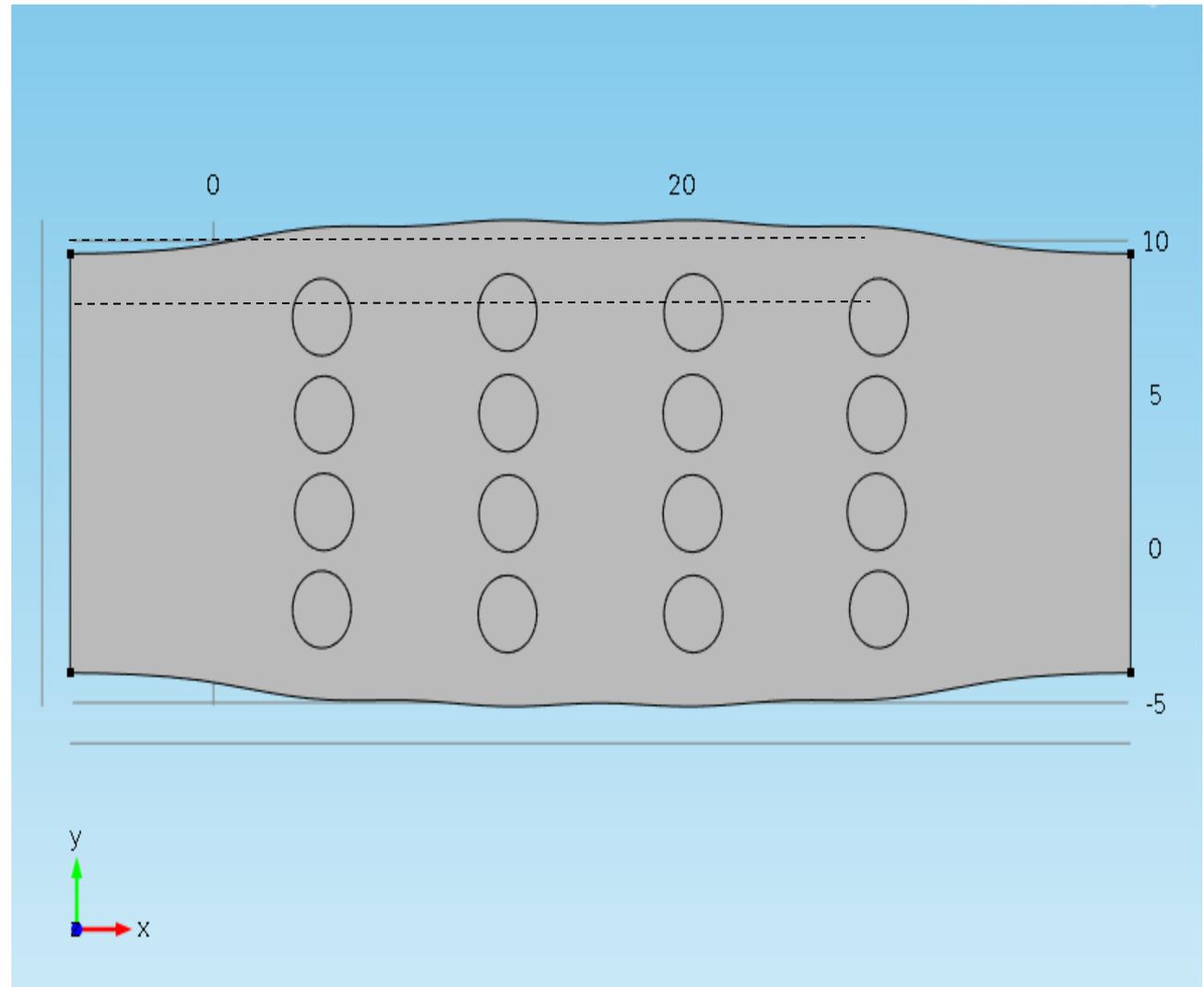
- ❖ Horizontal mechanical field (ABAQUS)
- ❖ Vertical electrical field (COMSOL)
- ❖ Can we make a 1:1 association between the distinguishing features of damage development and changes in dielectric properties, e.g., capacitance?



Nonlinear deformation:

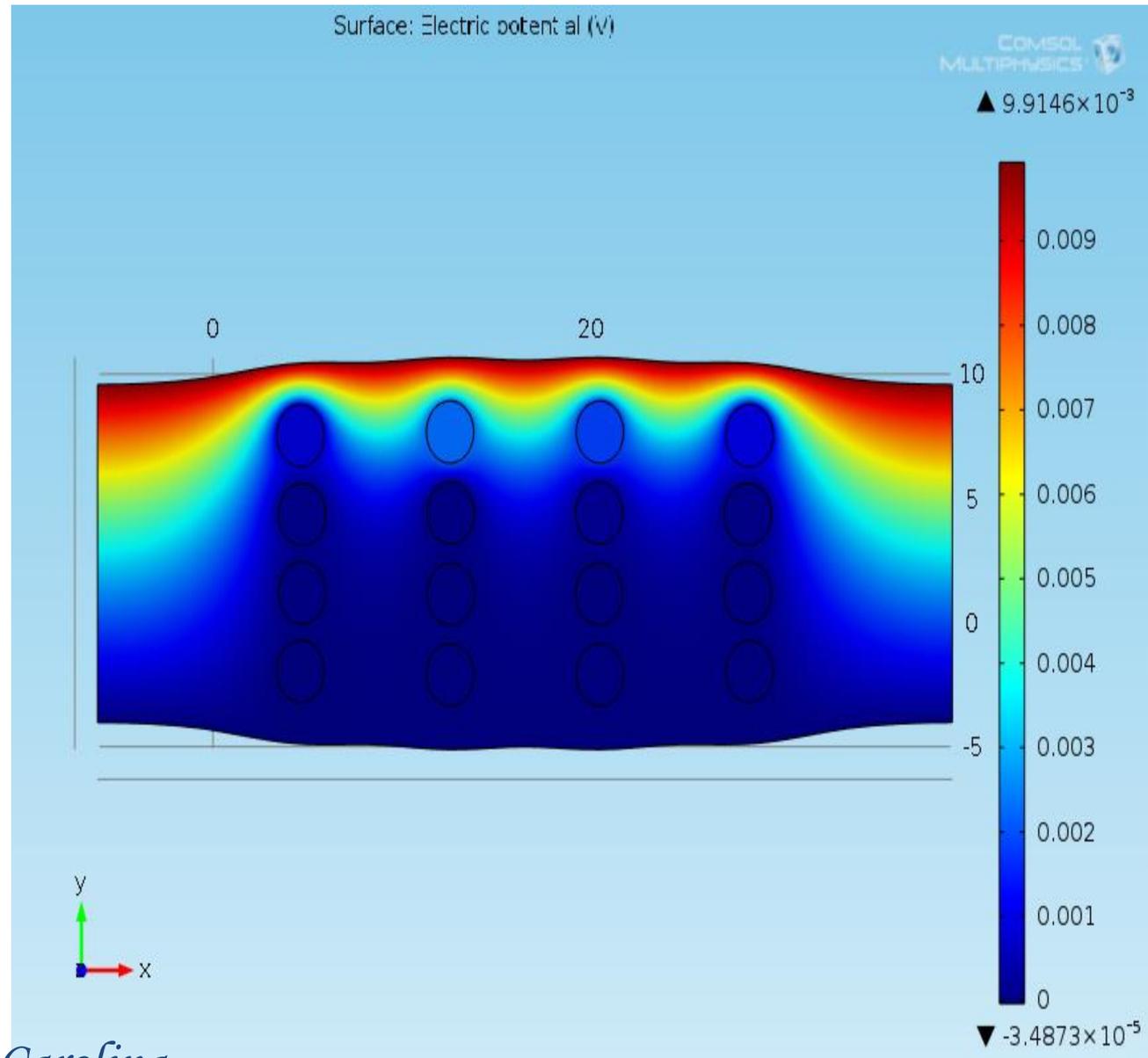
125% Strain

❖ Horizontal mechanical field (ABAQUS)



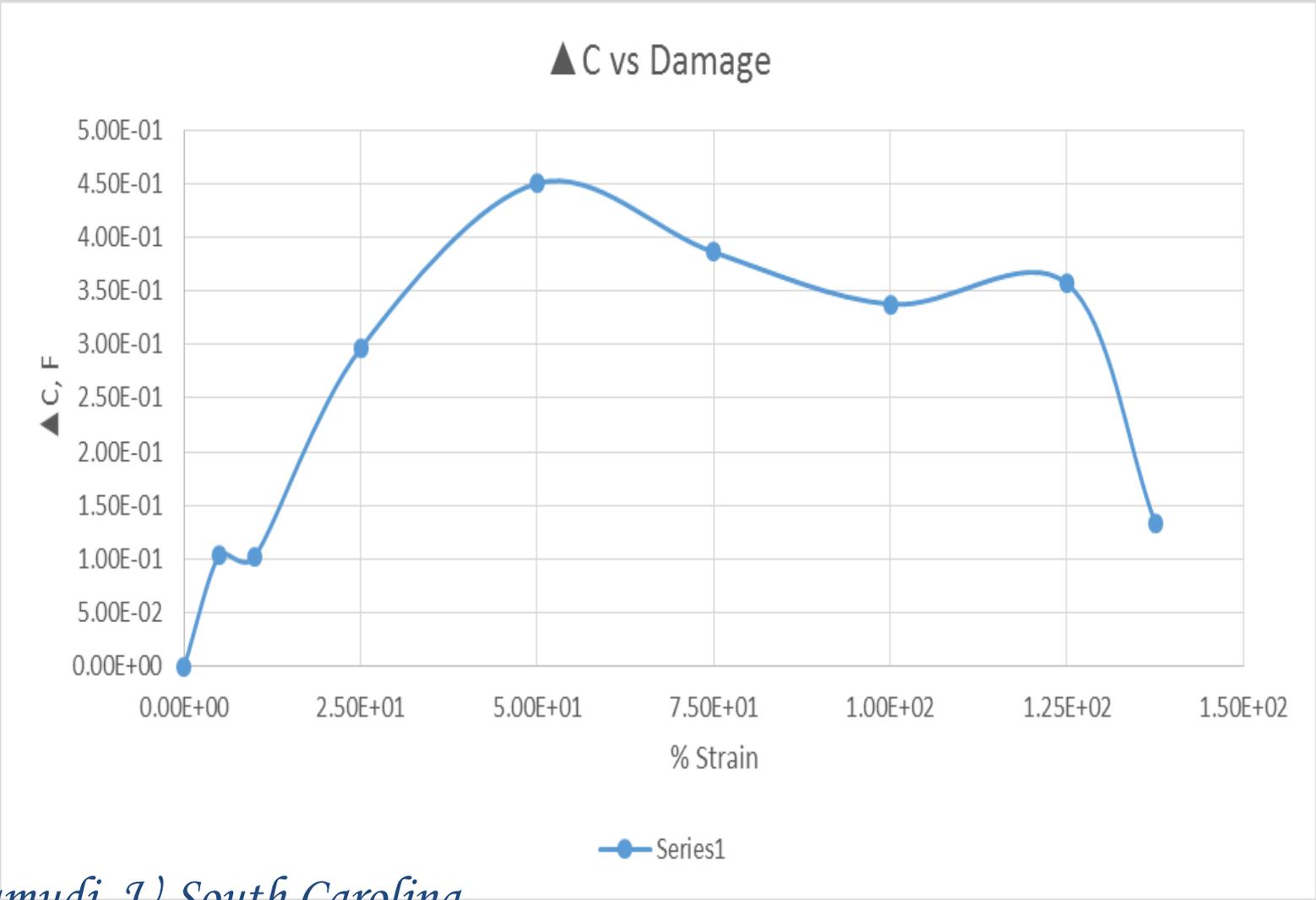
Nonlinear deformation:

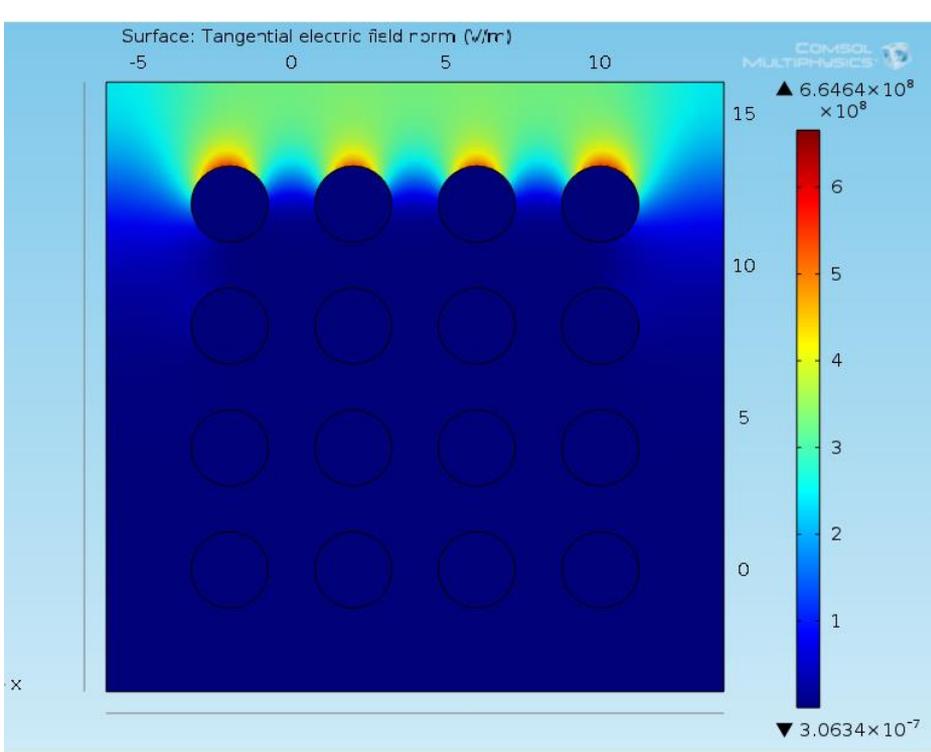
- ❖ Vertical (through the thickness) electrical field
- ❖ Internal charge accumulations interact – nonlinear results → can detect changes in response (slopes)



Nonlinear deformation:

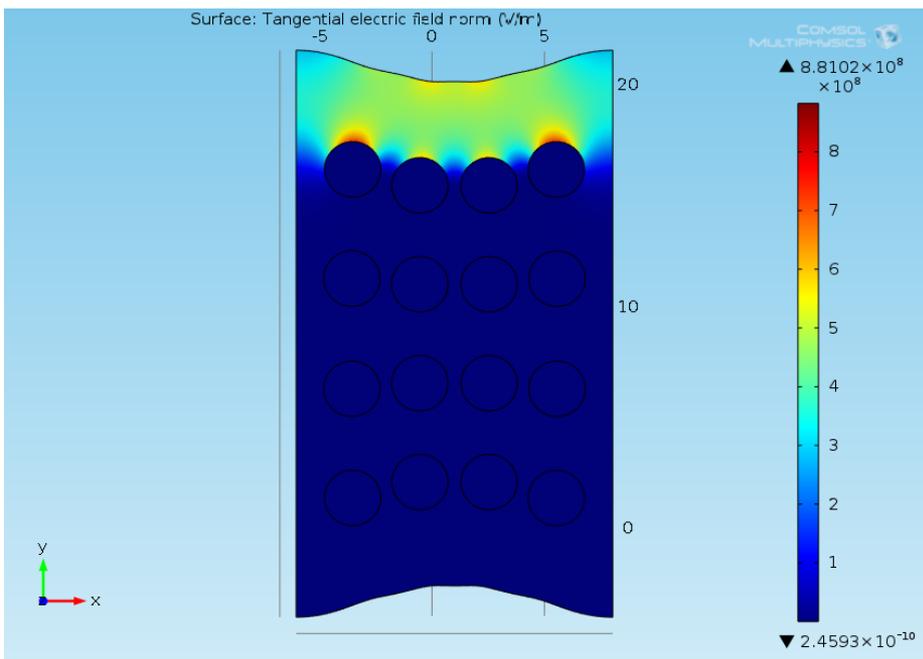
❖ Distinctive features of nonlinear deformation revealed in capacitive response:



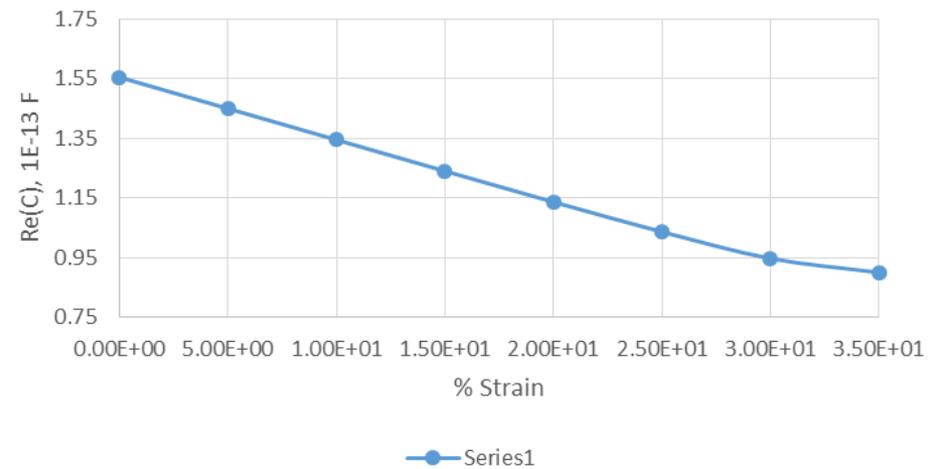


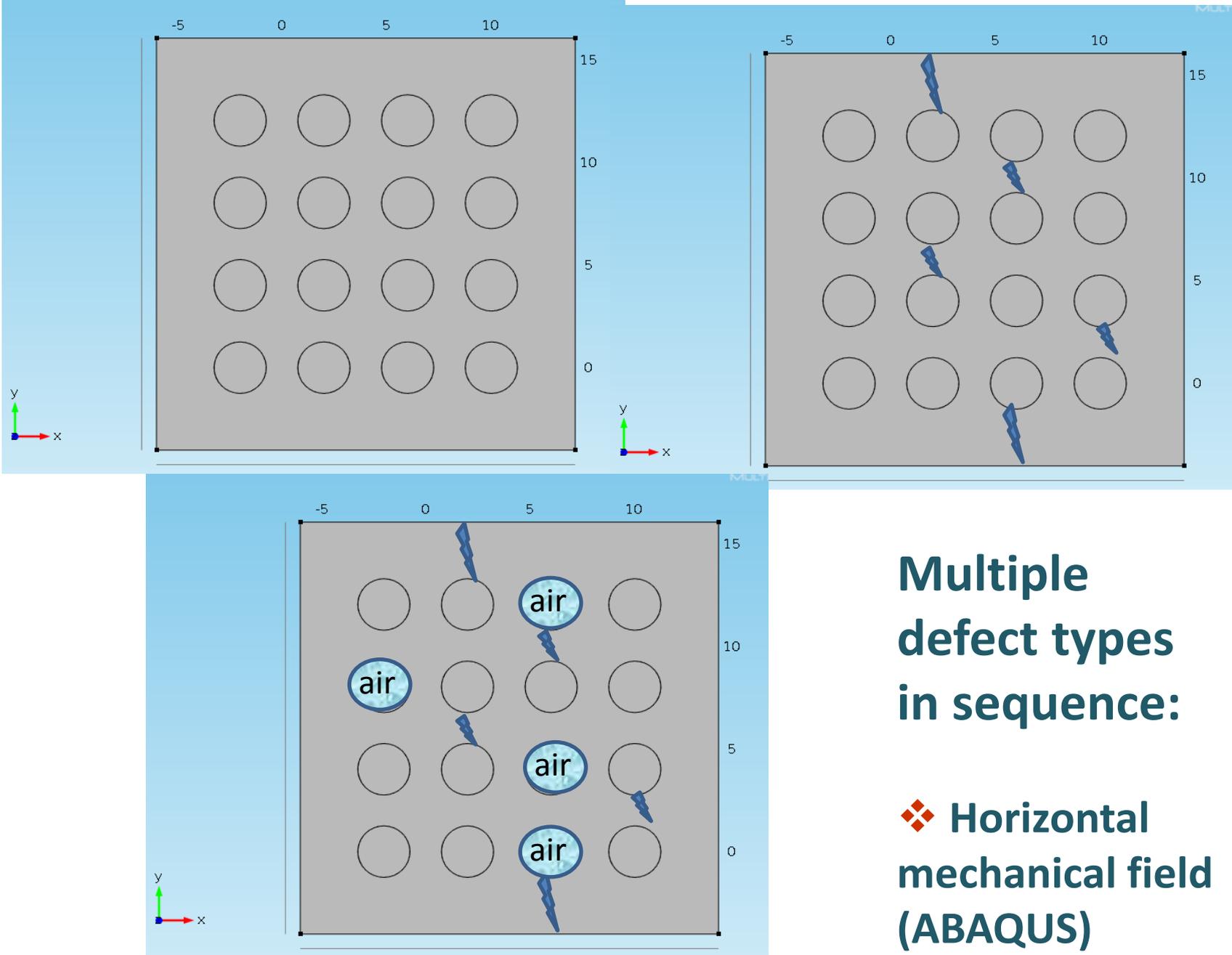
Nonlinear deformation:

❖ Compression is different than tension!



Compressive Strain Vs $Re(C)$





**Multiple
defect types
in sequence:**

❖ **Horizontal
mechanical field
(ABAQUS)**

Foundation for Predictive Methodology:

We can conduct simulations that combine predicted deformation patterns (e.g. with ABAQUS) that are directly used to predict concomitant changes in dielectric observables (e.g. with conformal models in COMSOL).

Specific damage modes are clearly and uniquely identified

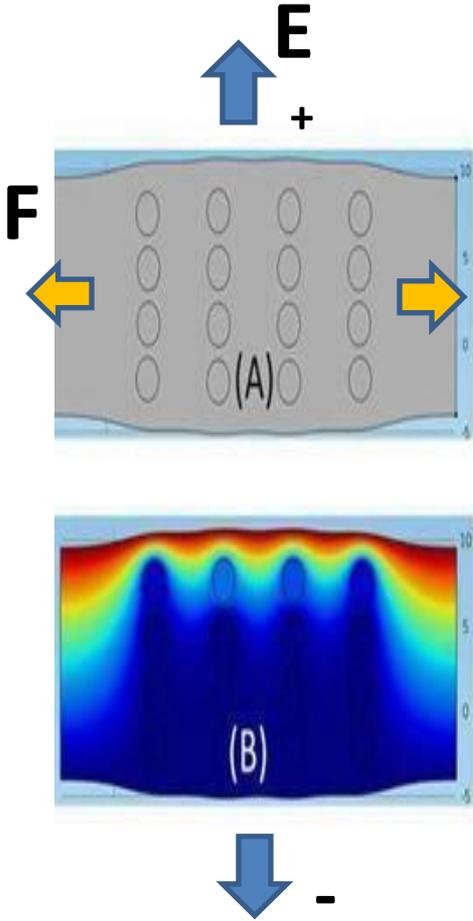
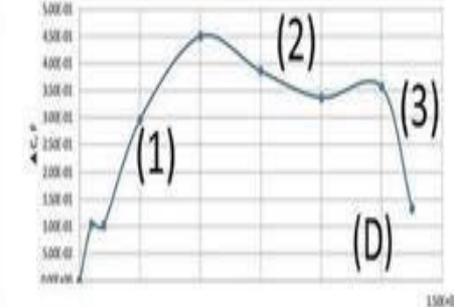
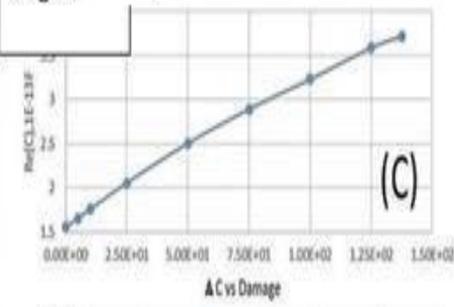


Fig. 3 Capacitance vs. Strain



Rate of change vs. Strain

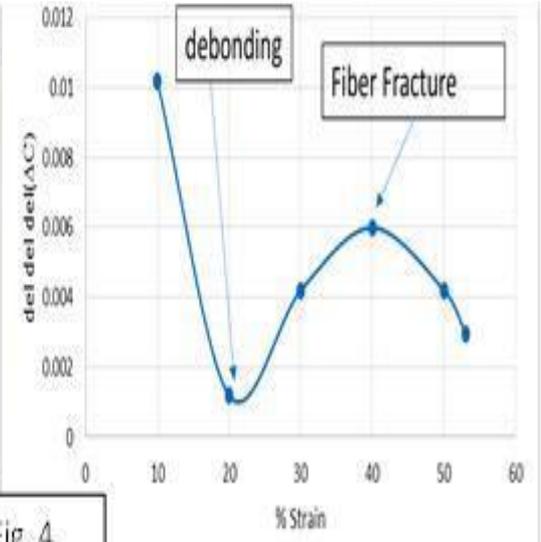
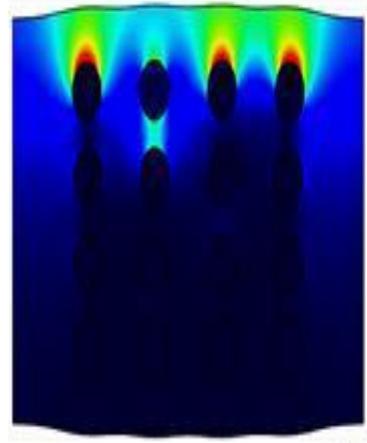


Fig. 4

1. K. Reifsnider, D. Cacuci, J. Baker, J. Adkins, F. Rabbi, "Validated predictive computational methods for surface charge in heterogeneous functional materials: HeteroFoaM,™ *Mechanics of Advanced Materials and Modern Processes* 2015, 1:3 doi:10.1186/s40759-014-0001-y

V. Vadlamudi, U South Carolina & K. Reifsnider, UTA

Institute for Predictive Performance Methodologies

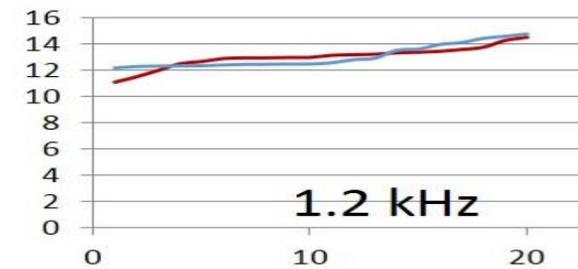
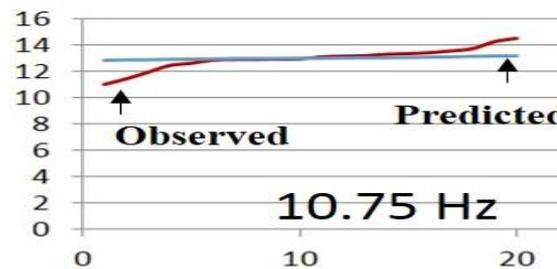
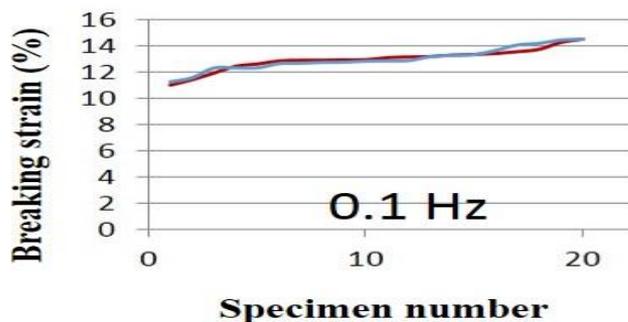
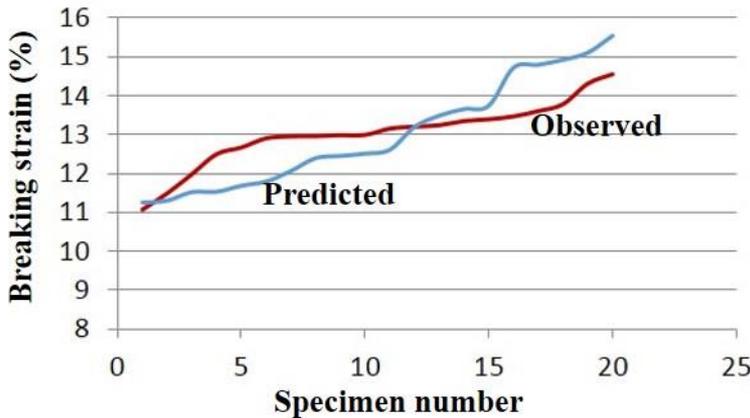


DIELECTRIC CURRENT STATE ANALYSIS FOR DURABILITY PROGNOSIS AND DESIGN OF COMPOSITE MATERIALS

If we rank the initial dielectric response, then rank the break strains; we find that the break strains of individual specimens predicted by multiplying the average strain for all specimens by the dielectric fraction for an equal rank is an excellent estimate of strength of each specimen.

“Current State Analysis Method”

Observed and predicted values of strain to break for 20 individual specimens based on initial values of the imaginary part of the permittivity measured through the thickness of those individual specimens before load application for different input frequencies



Multi-Scale Design and Prognosis of Multifunctional Composite Materials:

The concept -

Design



Detect



Predict

- **Multi-functional:** mechanical, thermal, electrical...
- **Multi-scale**
- **Nonlinear**
- **Non-conservative**

- **Material state:** dielectric, mechanical..
- **Defect state,** morphology, locations
- **Properties,** functionality

- **Performance,** reliability, risk:
- **Remaining strength,** life, stiffness, conductivity..
- **Functionality**
- **Risk / repair**



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- the broadband dielectric spectroscopy and related work from the Energy Frontier Research Center for Heterogeneous Functional Materials, the HeteroFoam Center, under DoE Grant no.DE-SC0001061 from the Office of Basic Energy Sciences
- Laboratory and facilities support from the USC SmartState Center for Solid Oxide Fuel Cells (www.sofccenter.com)
- The support of the Institute for Predictive Methodologies, UTA

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1. Reifsnider, K.L and Case, S., Damage tolerance and durability of material systems, John Wiley and Sons, New York, 2002
2. K. Reifsnider, D. Cacuci, J. Baker, J. Adkins, F. Rabbi, "Validated predictive computational methods for surface charge in heterogeneous functional materials: HeteroFoaM,TM *Mechanics of Advanced Materials and Modern Processes* 2015, **1**:3 doi:10.1186/s40759-014-0001-y
3. Raihan, R., Adkins, J. M., Baker, J., Rabbi, F., & Reifsnider, K. (2014). Relationship of dielectric property change to composite material state degradation. *Composites Science and Technology*, 105, 160-165.
4. K. L. Reifsnider, P. K. Majumdar and P. J. Fazzino, "Material state changes as a basis for prognosis in aeronautical structures," *J. Aeronautical Society*, vol. 113, no. 1150, pp. 789-798, 2009
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6. Raihan, R., Reifsnider, K., Cacuci, D., and Liu, Q., "Dielectric signatures and interpretive analysis for changes of state in composite materials," *J. Applied Mathematics and Mechanics (ZAMM)*, 1–9 (2015) / DOI 10.1002/zamm.201400226
7. Q. Liu and K. Reifsnider, "Heterogeneous mixtures of elliptical particles: directly resolving local and global properties and responses," *Journal of Computational Physics* (2012), oi.org/10.1016/j.jcp.2012.09.039
8. Q. Liu, "Physalis method for heterogeneous mixtures of dielectrics and conductors: Accurately simulating one million particles using a PC," *J. Comput. Phys.* 230, 8256 (2011)
9. J. Baker, J. M. Adkins, F. Rabbi, Q. Liu, K. Reifsnider and R. Raihan, "Meso-design of heterogeneous dielectric material systems: Structure property relationships," *Journal Of Advanced Dielectrics*, Vol. 4, No. 2 (2014), DOI:10.1142/S2010135X14500088
10. R. Raihan, " Dielectric Properties of Composite Materials during Damage Accumulation and Fracture," Dissertation, Mechanical Engineering, University of South Carolina, 2014
11. V. Vadlamudi, "Predictive Methods for End of Life Prognosis in Composites," MS thesis, Department of Mechanical Engineering, Univ. of South Carolina, 2015.

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1. Rassel Raihan, Jon-Michael Adkins, Jeffrey Baker, Fazle Rabbi, Kenneth Reifsnider; "Relationship of Dielectric Property Change to Composite Material State Degradation" Composite Science and Technology, Submitted
2. J. Baker, M. Haidar, R. Raihan, K. Reifsnider, "Effect of Manufacturing on the Dielectric Properties of Composite Materials." Proc. Am. Soc. Composites, U. Michigan, September, 2015
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4. R. Raihan, Q. Liu, K.L. Reifsnider, F. Rabbi; "Nano-Mechanics foundations and experimental methodologies for multiphysics prognosis of functional behaviour in heterogeneous functional materials (HeteroFoam)", Procedia IUTAM (2012)
5. R. Raihan, K. Reifsnider, Fazle Rabbi, Jeffrey Baker, Jon-Michael Adkins, Q. Liu," A Dielectric Spectroscopy Method of Directly Assessing Composite Micro-State Evolution During Manufacturing and Deformation" Society for the Advancement of Material and Process Engineering (SAMPE), Long Beach 2013
6. Md Rassel Raihan, Kenneth L Reifsnider;" Generalized Compliance, A New Technique for Progressive Damage Analysis in Composite Materials" The 19th International Conference on Composite Materials, Montreal 2013
7. Reifsnider, K. L.; Raihan, R.; and Liu, Q.;" Rational durability design of heterogeneous functional materials: Some first principles" Mechanics of Composite Materials, 49, 31-53, (2013)
8. P. Majumdar, M. Raihan, K. Reifsnider and F. Rabbi, "Effect of Porous Electrode Morphology on Broadband Dielectric Characteristics of SOFC and Methodologies for Analytical Predictions" Proc. ASME 2011 9th Fuel Cell Science Engineering and Technology, Aug. 2011
9. K. Reifsnider, R. Raihan, and P. Majumdar, "Durability Methodologies for Material Systems," Proc. PVP2011, July 2011